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# SUBMERGED SPRINGS SITE DOCUMENTATION: AUGUST AND SEPTEMBER 2007



# Submerged Springs Site Documentation: August and September 2007



For:

# St. Johns River Water Management District

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# Submerged Springs Site Documentation: August and September 2007

# **INTRODUCTION**

The St. Johns River Water Management District (SJRWMD) contracted with Karst Environmental Services, Inc. (KES) to assist in ground-truth investigations and the site documentation of various submerged springs and other undocumented sites that were identified as possible groundwater discharge locations by aerial thermography. KES also provided assistance to the SJRWMD and USGS with water sample collection for water quality analysis, and conducted discharge measurements as part of the Silver Springs Characterization Project.

#### PURPOSE and SCOPE OF WORK

The purpose and objective of this work was to:

- 1. Collect additional water quality samples, perform discharge measurements, and document measurement point conditions at 5 submerged spring vents of the Silver Springs Group and in the Silver River as part of the Silver Springs Characterization Project.
- 2. Provide submerged spring point documentation of groundwater discharges at one location in Blue Spring Run (Volusia County), three areas in the Silver River, and as many sites that could be visited for locations identified in the Wekiva River, Crescent Beach Spring, Shands Bridge Spring, the Rodman Reservoir and Ocklawaha River, Lake Harris and near Driggers Island in the St. Johns River.

The following tasks were to be performed at numerous locations within the District:

- 1. Spring Point Documentation at all located spring vents.
- 2. Water Quality Sampling at selected springs.
- 3. Spring Flow Measurements and Spring Flow Measurement Point Documentation at selected previously measured springs, and at un-measured springs investigated during this study that were suitable for the application of KES underwater measurement techniques.

#### PERSONNEL

Fieldwork was conducted by Peter Butt, Project Manager, Tom Morris, Biologist, and Mark Long, Field Technician. Videography was performed by Mark Long. Data management and report preparation was performed by Peter Butt and Tom Morris. Video was processed, edited and annotated by Georgia Shemitz.

# **METHODS**

The fieldwork for this study was carried out during the months of August and September, 2007.

GPS positions were taken from GIS imagery, and confirmed or corrected in the field. The latitude and longitude presented herein is in WGS84, and the UTM Easting and Northing data is in meters, and in UTM Zone 17, NAD 1983 HARN.

Physical measurements of the springs were taken using fiberglass tape and underwater compass, with data recorded on plastic slates.

Underwater video was taken at each site where spring vents were present.

At selected Silver Springs Group sites and at Shands Bridge Spring, KES divers assisted SJRWMD and USGS personnel in collecting water samples from individual spring vents. Samples were collected by divers running tubing connected to pumps on watercraft directly into spring vents. Water was analyzed on-site for field parameters and collected samples were sent by SJRWMD and USGS to labs for further analysis.

Discharge measurements were taken at selected spring vents. These measurements were taken using an electronic flowmeter adapted for underwater use. Three of the springs were measured using the standard cross-section method used by KES. Three springs (discharging through soft bottom sediments and algae) that did not lend themselves to this method were measured using a Vent Discharge Capture Device specially designed for this purpose. Data was processed using Golden Surfer 8 software. The results and summary of these measurements are presented under separate cover.

A brief narrative description of each of the various springs or spring groups is presented herein.

#### SITE DESCRIPTIONS

#### Rodman Reservoir/Ocklawaha River Springs

These following Rodman Reservoir/Ocklawaha River spring sites were all visited on August 29, 2007 by Pete Butt, Tom Morris and Mark Long, accompanied by Jeff Davis of the SJRWMD.

#### **Blue Spring (Marion County)**

Marion County N 29.514404°, W 81.856850° UTM 416958 E, 3265285 N Description:

This is the most downstream of the spring vents visited in Rodman Reservoir. This spring lies within a basin with a steeply sloping north (and shoreward) side. Strands of aquatic vegetation extending from the bottom to the surface were present. No boil was visible on the surface during the August 29 and September 27, 2007 visits, but a thermocline was present. The spring has two distinct vents discharging from bedrock, both too small for a diver to enter. The upper vent is an elongated irregular opening, with a horizontal cross-section about 1.5 feet wide by about 5.5 feet long, and begins at a depth of 29 feet. The lower vent is located directly below the upper vent, in about 33 feet of depth. This vent has a vertical cross-section of about 3 feet wide by 2 feet high, and is roughly triangular in shape. A large timber was lying above the vents. Silt around the vents was easily disturbed.



Figure 1. Underwater video still of Blue Spring (Marion County). View of the upper vent measurement cross-section.



Figure 2. Underwater video still of Blue Spring (Marion County). View of the lower vent.

#### **Bright Angel Spring**

Marion County N 29.516572°, W 81.862090° UTM 416452 E, 3265529 N Description:

This spring lies within a large basin about 30 feet in diameter about 560 meters northwest of Blue Spring. Timbers of various sizes are scattered about the bottom. No boil was visible on the surface during the August 29 and September 27, 2007 visits. A thermocline was present, at about 9 to 10 feet deep, with clear water below. The spring has one long vent discharging south to north from bedrock, and is too small for a diver to enter. The vent is at least 10 feet wide, with a horizontal cross-section about 1.5 feet high at its eastern side, and tapering down to a few inches high at its west end. The top of the vent is at about 24 feet of depth, and the bottom is at 26 feet deep. The bottom of the vent is composed of loose rock, rubble and silt. Silt around the vent was easily disturbed.



Figure 3. Underwater video still of Bright Angel Spring, Marion County, Florida. The diver is illuminating the higher eastern side of the vent.

# **Catfish Spring**

Marion County N 29.515419°, W 81.861750° UTM 416484 E, 3265401 N Description:

This spring lies in an area of heavy aquatic vegetation about 132 meters south of Bright Angel Spring and about 485 meters west-northwest of Blue Spring. No boil was visible on the surface during the August 29 visit. The spring has one vent discharging from bedrock, too small for a diver to enter. The vent was at about 18 to 20 feet of depth. Discharge from this vent was very weak.



Figure 4. Underwater video still of Catfish Spring, Marion County, Florida.

# **Bamboo Spring**

Marion County N 29.515847°, W 81.866716° UTM 416003 E, 3265452 N Description:

This spring lies in an area of heavy aquatic vegetation about 450 meters west of Bright Angel Spring. The vent was located in an area marked by bamboo poles stuck into the bottom, apparently as markers for fisherman. No boil was visible on the surface during the August 29 visit. This spring had a cluster of small vents discharging from vegetated soft sediments. The vent area is at about 8 feet of depth. Discharge from this spring was very weak.



Figure 5. Underwater video still of Bamboo Spring, Marion County, Florida.

# **Trench Seep**

Marion County N 29.516670°, W 81.868330° UTM 415842 E, 3265531 N Description:

This seep area is located in an area of heavy aquatic vegetation northwest of Bamboo Spring. The clear, cooler water that identifies the seep area was located in channels between areas of thick aquatic vegetation. No actual vents were visible during the August 29, 2007 visit. This seep apparently discharges through vegetated soft sediments. The seep area is at about 10 feet deep.



Figure 6. Underwater video still of Trench Seep, Marion County, Florida. This view is typical of bottom conditions in the cool water areas.

# Sim's Spring

Marion County N 29.508108°, W 81.892010° UTM 413545 E, 3264613 N Description:

Sim's Spring is identified by its surrounding man-made concrete structure, which apparently contained the spring and functioned as a control structure. A walkway leads up the shore slope to a small building that appears to have been a pump house. The pool within the concrete structure was searched, and although bedrock could be seen, there was no apparent discharge. Water depth was about 4 feet deep during the August 29, 2007 visit.



Figure 7. Video still of Sim's Spring, Marion County, Florida. The apparent vent is under the concrete wall on the left. The vertical slot behind the diver on the right is a discharge control structure.

#### Fish Hook Spring #1

Marion County N 29.509479°, W 81.901514° UTM 412625 E, 3264772 N Description:

This spring lies in an area of heavy aquatic vegetation along the south shore of the reservoir, and about 91 meters east of Fish Hook Spring #2. No boil was visible on the surface during the August 29 visit. This spring has one vent of less than 2 feet in diameter discharging from bedrock and loose rock through soft sediments. The vent is about 8 feet deep. Discharge from this vent was very weak.



Figure 8. Underwater video still of Fish Hook Spring #1, Marion County, Florida.

#### Fish Hook Spring #2

Marion County N 29.509041°, W 81.902304° UTM 412548 E, 3264724 N Description:

This spring lies in an area of heavy aquatic vegetation along the south shore of the reservoir, and about 91 meters west of Fish Hook Spring #1. No boil was visible on the surface during the August 29 visit. This spring has a vent area of about 10 feet in diameter discharging from bedrock through a jumble of loose rock and timbers. The vent is about 8 feet deep. Discharge from this vent was weak.



Figure 9. Underwater video still of Fish Hook Spring #2, Marion County, Florida. Shown is one of several vents discharging through a jumble of loose rock and timbers

#### **Floating Dock Anomaly**

Marion County N 29.512660°, W 81.868350° UTM 415842 E, 3265100 N Description:

The area searched lies within a bay along the south shore, and near some docks and piers. The bay is in an area of heavy aquatic vegetation. No obvious spring vents, seeps or areas of cooler water were located after extensive snorkeling of the area.

These following Rodman Reservoir/Ocklawaha River spring sites were all visited on August 30, 2007 by Pete Butt, Tom Morris and Mark Long, accompanied by Jeff Davis of the SJRWMD.

#### No-Name Seep #2

Marion County N 29.501785°, W 81.912804° UTM 411524 E, 3263928 N Description:

This seep area lies in an area of heavy aquatic vegetation. The clear, cooler water that identifies the seep area was located in open areas surrounded by thick aquatic vegetation. The seep formed a cool water layer about a foot thick over the bottom, and no actual vents were visible during the August 30, 2007 visit. This seep apparently discharges through vegetated soft sediments. The seep area is at about 6 feet deep.

#### No-Name Seep #3

Marion County N 29.506118°, W 81.910047° UTM 411795 E, 3264406 N Description:

This seep area lies in an area of heavy aquatic vegetation. The clear, cooler water that identifies the seep area was located in open areas surrounded by thick aquatic vegetation. The seep formed a cool water layer about a foot thick over the bottom, and no actual vents were visible during the August 30, 2007 visit. This seep apparently discharges through vegetated soft sediments. The seep area is at about 5 feet deep.

# Lake Harris Springs

These following Lake Harris spring sites were all visited on September 12, 2007 by Tom Morris and Mark Long, accompanied by Jeff Davis of the SJRWMD.

# Site 1 Spring Pool and Outfall

Lake County N 28.746550°, W 81.798470° UTM 422039 E, 3180167 N Description:

The Site 1 Spring Pool and Outfall is located along the southern shoreline of Lake Harris. The assumed spring pool is several hundred feet from the lake, in a mature forested wetland (bayhead). The circular pool was about six feet across and six feet deep and contained cool and slightly tannic water, but no vents were found. Discharge from the pool appears to flow down a small heavily vegetated channel excavated during the construction of a small causeway through the wetland. No discharge was apparent from the pool on September 12, 2007. However, farther downstream, water was flowing fairly vigorously from the bayhead into the littoral zone of the lake. This suggests that the site may be an area of general groundwater seepage, or that undetected vents are hidden in the vegetation of the drainageway.



Figure 10. Video still of Lake Harris Site 1 Spring Pool, Lake County, Florida.

# **Dock Spring**

Lake County N 28.748366°, W 81.802416° UTM 421655 E, 3180371 N Description:

Dock Spring is located along the southern shoreline of Lake Harris, within the littoral zone. The cool water of the spring discharges into a metal casement, about four feet in diameter and five feet tall, that has been placed over the spring. The pipe, which is attached to a dock, acts as a reservoir for a small watering system. The water surface in Lake Harris was low at the time of the visit, and the pipe was just at the waterline. Nonetheless, the water level in the pipe was about three feet above the water level in the lake.



Figure 11. Video still of Lake Harris Dock Spring, Lake County, Florida. Spring is encased in large diameter steel casing below pumps on right side of picture.

# **Twin Sand Boils Spring**

Lake County N 28.747431°, W 81.804908° UTM 421411 E, 3180269 N Description:

Twin Sand Boils Spring is located in the littoral zone of the southern shoreline of Lake Harris. This feature consists of two small sand boils, each several inches in diameter and about a foot apart, in an area of very shallow water (less than 0.5 feet) and somewhat sparse emergent vegetation. The cool temperature of the discharge relative to the warm lake water suggests a groundwater source.



Figure 12. Video still of Lake Harris Twin Sand Boils Spring, Lake County, Florida.

# **Cypress Tree Seep**

Lake County N 28.748069°, W 81.803837° UTM 421516 E, 3180339 N Description:

Cypress Tree Seep is located in the littoral zone of the southern shoreline of Lake Harris. This feature is an area of notably cool water, no more than several inches deep, and about ten feet in diameter. No vent was found, but the relatively cool temperature of the seep area, when compared with the surrounding warm water of the lake, indicates discharge of groundwater. The shallow water in and around the seep supports emergent vegetation, and the feature is named after a nearby cypress tree.



Figure 13. Video still of Lake Harris Cypress Tree Seep, Lake County, Florida.

# Sandy's Spring

Lake County N 28.745080°, W 81.810154° UTM 420897 E, 3180012 N Description:

Sandy's Spring is located at the head of a small run about 200 feet from the southern shoreline of Lake Harris. The spring run discharges into the littoral zone of the lake after flowing through a small culvert under Lakeshore Drive. The spring vent is located in a roughly circular pool, which is about ten feet in diameter, and about six feet deep. Groundwater gently discharges from a linear vent about two feet long at the deepest part of the spring pool. The vent was partially covered by soft sediments. The spring pool and run are maintained by the owner and are free of aquatic vegetation.



Figure 14. Video still of Sandy's Spring pool, Lake County, Florida.



Figure 15. Underwater video still of Sandy's Spring, Lake County, Florida. The vent at the deepest part of the pool is shown.

# **Crescent Beach Spring**

St. Johns County N 29.768295°, W 81.207945° UTM 479898 E, 3293129 N Description:

Crescent Beach Spring was visited on August 30, 2007 by Peter Butt, Tom Morris and Mark Long. Jeff Davis of the SJRWMD arranged for a District work boat and crew, and provided surface support. A video of the dive here was made.

Upon arrival at the site, a prominent and very cloudy boil, or slick, was present on the ocean surface. The boat was anchored in the depression, and the divers descended down the anchor line to the bottom. Upon reaching the bottom, visibility was extremely limited, and a guideline reel was affixed to the anchor line and a sweep was made of the bottom, at depths reaching 130 feet. The water here was very agitated and filled with suspended sediments. The search of the bottom was by feel, and only soft and clay-like sediments and bivalve shells were found. No direct contact was made with any identifiable vents, either visually or by feel.

After exploring the bottom of the depression, the divers ascended the anchor line to about 65 feet deep and then ran a guideline laterally until making contact with the bottom. The divers swam radially, exploring the sloping sides of the depression at 60 to 70 feet of depth. The bottom consisted of soft sediments. No natural bottom structure was encountered that would allow for support of an underwater discharge measurement, and visibility was problematic.

# **Shands Bridge Spring**

St. Johns County N 29.988461°, W 81.623216° UTM 439885 E, 3317670 N Description: Shands Bridge Spring was visited

Shands Bridge Spring was visited on August 31, 2007 by Peter Butt, Tom Morris and Mark Long. Jeff Davis of the SJRWMD arranged for a District work boat and crew, and provided surface support. A video of the dive here was made.

Shands Bridge Spring is located in depression in the approximate middle of the St. John's River, downstream of Shands Bridge. No boil or slick was visible during this visit. The general location of the site was located using a depth finder, and then divers found the vent by following water temperature, bottom topography and debris. The spring vent was located beneath a derelict wire crab trap, and discharged up through the trap, at about 28 feet deep. A thick layer of soft organic sediments containing considerable man-made debris surrounded the vent (and crab trap) at the bottom of the depression. The vent could only be viewed by looking down through the upper end of the crab trap, and even then, the vent below was obscured by debris and sediment.

A water sample was collected by divers placing the end of an intake tube through the top of the crab trap and into the clear water directly above the vent.



Figure 16. Underwater video still of Shands Bridge Spring, St. Johns County, Florida. Beam of light is shining down through the crab trap to the debris choked vent below.

# **Driggers Island Hole, St. Johns River**

Volusia County N 28.998834°, W 81.377810° UTM 463201 E, 3207915 N Description:

Driggers Island Hole is a large depression, over sixty feet deep, in the bottom of the St. Johns River, downstream of the Hwy 44 bridge. This feature had been previously located by KES personnel with a depth finder, and its unusual depth suggested the possibility of groundwater discharge. Morris and Long explored the area with SCUBA on September 12, 2007. Jeff Davis of the SJRWMD provided surface support. The divers entered the water from a boat about fifty feet from the east bank and, with the aid of an underwater guideline, explored the river bottom almost over to the west bank, looking for relatively cool and clear groundwater. The maximum depth of the feature was 63 feet deep, and there was no ambient light below about fifteen feet deep. The bottom was composed of soft organic sediments. No groundwater discharge was found. As no groundwater discharges were located here, no photographs or video was taken at the site.

#### Wekiva River Upstream of Highway 46 Bridge

A section of the Wekiva River upstream of Highway 46 Bridge was visited on August 9, 2007 by Peter Butt, Tom Morris and Mark Long. Jeff Davis and Stan Williams of the SJRWMD provided surface support and watercraft. The only video of activity made here was of a large fossil bone that was forwarded to state park personnel.

Numerous anomaly sites that were identified by aerial thermography as potential spring sites were thoroughly investigated using snorkeling gear. No springs or areas of identifiable groundwater discharge were found. This included the search of main and side channel areas. The only vent-like features observed were those created near the "old trestle" area in the clay bottom sediments by exotic armored catfish.

#### Blue Spring State Park; Recon of Main Spring and Spring Run/St. Johns River Confluence

The headspring, run and St. Johns River confluence of Blue Spring at Blue Springs State Park area was visited on August 8, 2007 by Peter Butt, Tom Morris and Mark Long. Jeff Davis and Stan Williams of the SJRWMD provided surface support and watercraft. A video of the dive activities in the cavern, run and confluence was made.

The Blue Spring cavern was dived to the bottom by Tom Morris and Mark Long. A maximum depth of 130 feet was reached at the high flow restriction. As the divers ascended, they investigated the sides of the cavern for additional incoming flow of groundwater, including a small side tunnel at about 25 feet deep; no additional flows were found. The high flow restriction at 130 feet deep is the only location through which water enters the cavern. The divers took compass azimuths of the joint alignments of the cavern. These were directly reported to SJRWMD staff.

All three divers investigated the entire length of the spring run, with special attention paid to areas identified by aerial thermography as potential spring vents; none were found.

The prominent anomaly signature area identified by aerial thermography as a potential spring site in the run/river confluence was thoroughly investigated using SCUBA gear. No depressional features, springs or areas of identifiable groundwater discharge were found. Several sweeps were made independently by all three divers, including moving along the river/spring run water interface. The sand/silt bottom was relatively featureless, with widely scattered man-made debris, shell and rubble. Bottom relief was gentle, with a maximum depth of about 17 feet. The water near the bottom in the search area had very good visibility due to the spring water discharging from the run.

# Silver River Below the Silver Springs Group

The section of the Silver River downstream of the Silver Springs Group and the 1200 meter gauging station was visited on August 10, 2007 by Peter Butt and Tom Morris. Jeff Davis and Stan Williams of the SJRWMD provided surface support and watercraft. No video of activity here was made.

Numerous anomaly sites that were identified by aerial thermography as potential spring sites were thoroughly investigated using SCUBA and/or snorkeling gear. No springs or areas of identifiable groundwater discharge were found. This included the search of a channel and pond area on the south side of the river. The only vent-like features observed were those created in the clay bottom sediments by exotic armored catfish.

# Silver Springs Group Channel and Boat House Vents

#### Gang of 5 Vent #1

Marion County N 29.213593°, W 82.052945° UTM 397652 E, 3232109 N Description:

The Gang of Five Vent Group lies within a boat channel about 100 meters northeast of the boat house area, and about 60 meters south of a tourist boat dock located on one of the park's islands. All of these vents are approximately 10 feet deep. All discharge directly from bedrock, with varying amounts of loose rock, shells, sand, and dead wood (branches) in them. Vent #5 was the smallest, and the most difficult to collect water samples from.



Figure 17. Underwater video still of Gang of 5 Vent #1, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

**Gang of 5 Vent #2** Marion County N 29.213592°, W 82.053058° UTM 397641 E, 3232109 N



Figure 18. Underwater video still of Gang of 5 Vent #2, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

Gang of 5 Vent #3 Marion County N 29.213646°, W 82.053058° UTM 397641 E, 3232115 N



Figure 19. Underwater video still of Gang of 5 Vent #3, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

Gang of 5 Vent #4 Marion County N 29.213691°, W 82.053079° UTM 397639 E, 3232120 N



Figure 20. Underwater video still of Gang of 5 Vent #4, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

**Gang of 5 Vent #5** Marion County N 29.213637°, W 82.053079° UTM 397639 E, 3232114 N



Figure 21. Underwater video still of Gang of 5 Vent #5, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

# Sandboil Vent

Marion County N 29.214100°, W 82.051520° UTM 397791 E, 3232164 N Description:

This spring is a small sand boil located on the bottom of the channel, about 225 meters downstream of the boat house. It discharges through sand and soft bottom sediments about 10 feet deep.



Figure 22. Underwater video still of Sandboil Vent, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.
#### Silver Springs Landing Vent #1

Marion County N 29.215121°, W 82.046767° UTM 398254 E, 3232273 N Description:

These vents form a group, or cluster, in a deeper portion of the channel about 750 meters downstream of the boat house. They are located in front of a park re-creation of an old time Florida river trading post and river boats. They all discharge through sand, soft bottom sediments and heavy detritus at about 13 feet of depth. Vent #1 is the most northern of the vents, Vent #2 is mid-channel, and Vent #3 lies closest to the south bank. Vent #3 has the most aquatic vegetation around it.



Figure 23. Underwater video still of Silver Springs Landing Vent #1, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

# Silver Springs Landing Vent #2

Marion County N 29.215058°, W 82.046746° UTM 398256 E, 3232266 N



Figure 24. Underwater video still of Silver Springs Landing Vent #2, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

# Silver Springs Landing Vent #3

Marion County N 29.215013°, W 82.046745° UTM 398256 E, 3232261 N



Figure 25. Underwater video still of Silver Springs Landing Vent #3, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

# South Boat House/Christmas Boat Vent

Marion County N 29.212856°, W 82.053709° UTM 397577 E, 3232028 N Description:

This vent has two openings in the rocky bottom in front of the eastern side of the south (main) boathouse. Flow was vigorous from both openings. Aquatic vegetation surrounds the vent, which is 8 feet deep. The name references a glass-bottomed boat berthed nearby that has been outfitted with Christmas lighting.



Figure 26. Underwater video still of South Boat House/Christmas Boat Vent, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

#### South Boat House Vent #2

Marion County N 29.212856°, W 82.053688° UTM 397579 E, 3232028 N Description:

This vent is located under the roof of the south (main) boathouse in 8 feet of water, just southwest of the Christmas boat vent. The spring discharges from a bedrock vent obscured by sand, and is littered with debris.



Figure 27. Underwater video still of South Boat House Vent #2, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

#### South Boat House Vent #3

Marion County N 29.212856°, W 82.053678° UTM 397580 E, 3232028 N Description:

This vent is located under the roof of the south (main) boathouse in 8 feet of water, just west of Vent #2. The vent discharges from bedrock mantled by sand, and is littered with debris.



Figure 28. Underwater video still of South Boat House Vent #3, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

#### North Boat House/Rubber Mask Vent

Marion County N 29.212982°, W 82.053741° UTM 397574 E, 3232042 N Description:

This vent has multiple openings in the rocky bottom in front of (south of) the north boathouse. Flow was vigorous from all openings. Aquatic vegetation surrounds the vent openings, which are 8 feet deep. The name makes reference to a piece of man-made litter that was found during the investigation



Figure 29. Underwater video still of North Boat House/Rubber Mask Vent, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

# North Boat House/Silver Queen IV Vent

Marion County N 29.213054°, W 82.053762° UTM 397572 E, 3232050 N Description:

This vent is located under the roof of the north boathouse in 8 feet of water. The vent discharges from bedrock mantled with sand and debris. The name makes reference to an old river boat berthed above it.



Figure 30. Underwater video still of North Boat House/Silver Queen IV Vent, Silver Springs Group Channel and Boat House Vents, Marion County, Florida.

# **APPENDIX I**

#### Main Silver Springs Group Water Quality Sampling and Discharge Measurements

The following are spring descriptions and maps excerpted from "Silver Springs Spring Vent Documentation, Marion County, Florida; September, 2006", a report prepared by Karst Environmental Services, Inc. for SJRWMD in 2006 and 2007. These have been edited and are presented as support information relative to the Main Silver Springs Group Water Quality Sampling and Discharge Measurements made during September of 2007 by SJRWMD and USGS. All springs included below were sampled by a SJRWMD contactor on September 4, 2007 for specific parameters. Mammoth East and West, Catfish Hotel, Catfish Convention Hall and Lost River Springs were sampled by USGS personnel on September 5 and 6, 2007. Underwater discharge measurements were made at Mammoth, Catfish Convention Hall and Lost River Springs by KES personnel on September 10 and 11, 2007.

#### **Mammoth Spring**

Marion County N 29.216167°, W 82.052667° UTM 397670 E, 3232394 N Description:

This is the largest and most upstream of the spring vents. It discharges horizontally into a large basin just east of the glass-bottom boat loading area. The vent is a horizontal, oval-shaped opening 2 to 6 feet high and about 65 feet wide at the base of a limestone wall. The bottom of the vent's mouth is composed largely of breakdown boulders and rubble. The depth of water measured in front of the vent opening is about 34 feet. Water from at least two distinct sources (Mammoth East and Mammoth West) discharge from the cave opening. These sources differ in temperature and chemistry. The spring basin measures about 300 feet north to south and 200 feet east to west.



Figure 31. Mammoth Spring, Silver Springs Group, Marion County, Florida. Viewed from inside the cavern looking out. Discharge measurement supports are in place.



Figure 32. Map of Mammoth Spring, Silver Springs Group, Marion County, Florida.

# **Oscar Spring**

Marion County N 29.215283°, W 82.051533° UTM 397791 E, 3232294 N

Description:

Oscar Spring is a group of spring vents in a shallow depression on the north side of the center of the river channel, about 140 feet northeast of Jacob's Well Spring. There are three small vents in the depression, one of which discharges from a marl ledge, and a line of vents about 8 feet long about ten feet to the southwest of the marl ledge. The deepest part of the depression is about 17 feet deep.



Figure 33. Underwater photograph of Oscar Spring, Silver Springs Group, Marion County, Florida.



Figure 34. Map of Oscar Spring, Silver Springs Group, Marion County, Florida.

# Garden of Eden Spring Group

Description:

The Garden of Eden Spring Group is located in a cove about 240 feet east of Christmas Tree Spring. Garden of Eden is in the same cove as the jungle boat docks. A linear depression about 24 feet long and 15 feet deep contains a line of vents. This vent line accounts for most of the discharge from this group, and contains debris. About 30 feet west of this vent line, there is a roughly circular vent about 4 feet in diameter and 14 feet deep.

Another line of vents, about 17 feet long and 15 feet deep, lies 110 feet southwest of the main vent line. This vent line lies within a depression at the edge of the strong flow of the Silver River. The vents discharge through sand and gravel sediments.

# Lost River Spring and Log Spring

Marion County N 29.216267°, W 82.048200°

Description:

Two additional vents were discovered during this study east of the vent line, in a shallow swampy extension of the cove. The nearest of these, named Lost River Spring, is about 70 feet to the east, and is about two feet in diameter and about 8 feet deep. The second vent, named Log Spring, is 110 feet to the east of the vent line, and is about 3 feet in diameter and 5 feet deep. The vents of both of these springs gently discharge through detrital sediments and are beneath fallen tree limbs.



Figure 35. Underwater photograph of Lost River Spring, Silver Springs Group, Marion County, Florida.



Figure 36. Map of Garden of Eden Springs Group, including Lost River Spring, Silver Springs Group, Marion County, Florida.

#### No Name Cove Spring

Marion County N 29.215617°, W 82.046300° UTM 398298 E, 3232326 N

Description:

No Name Cove Spring is a line of six vents spread along the bottom of linear depression located in a small cove along the south side of the Silver River, about 450 feet east of First Fisherman's Paradise. The vents discharge vertically through soft bottom sediments, from between 10 to 14 feet deep.



Figure 37. Underwater photograph of No Name Cove Spring, Silver Springs Group, Marion County, Florida.



Figure 38. Map of No Name Cove Spring, Silver Springs Group, Marion County, Florida.

# **Catfish Hotel Spring**

Marion County N 29.215383°, W 82.0545050° UTM 398415 E, 3232301 N

Description:

Catfish Hotel Spring is located in the main channel approximately 100 feet southeast of Second Fisherman's Paradise Spring. This spring has a deep basin that is bordered on the east by a limestone ledge. West of this ledge is a large and complex area of angular boulders and slabs. Discharge was strong from the numerous vents scattered among the boulders and ledges. Void spaces below the rocks extend down past depths of 25 feet. The physical structure and complexity of this spring did not lend itself to the application of the underwater discharge measurement methods used at the other springs.



Figure 39. Underwater photograph of Catfish Hotel Spring, Silver Springs Group, Marion County, Florida.



Figure 40. Map of Catfish Hotel Spring, Silver Springs Group, Marion County, Florida.

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# **Shipwreck Springs Group**

# **Shipwreck Spring**

# Description:

The main vent of the Shipwreck Springs Group is located at the bow of a sunken boat on the bottom of a large, 20 foot deep depression north of the main river channel, and east of the eastern tip of a forested island. The main vent discharges from rock through a layer of sediment and algae. Another similar but smaller vent lies about 15 feet to the east. Discharging from the algae-covered bottom of the western side of the basin, and about 20 to 30 feet from the stern section of the sunken boat, are numerous small vents.

# **Catfish Convention Hall Spring**

Marion County N 29.215450°, W 82.0438667° UTM 398536 E, 3232306 N Description:

Catfish Convention Hall Spring is comprised of two clusters of small vents, about 20 feet deep, and located directly downstream from Shipwreck Spring and the bow of the namesake sunken boat. They lie in the eastern end of the basin that is an extension of the Shipwreck Spring basin. The main vent cluster contains about five small vents within an area of about six feet in diameter, all discharging through sediments.



Figure 41. Underwater photograph of Catfish Convention Hall Spring vents, Silver Springs Group, Marion County, Florida. This area contains the main vent cluster.



Figure 42. Underwater photograph of Catfish Convention Hall Spring, Silver Springs Group, Marion County, Florida. Vents that comprise this spring lie in front of the diver.



Figure 43. Map of Catfish Convention Hall Spring in the Shipwreck Springs Group, Silver Springs Group, Marion County, Florida.

#### **APPENDIX II**

Copy of "Twenty Springs of the Oklawaha. An Occasional Paper prepared for the Florida Defenders of the Environment, Inc." By Elizabeth F. Abbott, University of Florida Dept. of Geology. Gainesville, Florida Summer, 1971

The following 15 page report, "Twenty Springs of the Oklawaha" by Elizabeth F. Abbott, is reproduced herein for historical and reference purposes, and contains narrative descriptions, a list and map of springs, and references. This report was consulted during the Ocklawaha/Rodman Reservoir area fieldwork covered in this report. This copy of the report was provided by the SJRWMD library.

#### TWENTY SPRINGS OF THE OKLAWAHA

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Elizabeth F. Abbott

Department of Geology University of Florida Gainesville, Florida Summer, 1971

An Occasional Paper prepared for Florida Defenders of the Environment, Inc.

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#### TWENTY SPRINGS OF THE OKLAWAHA

An analysis of the hydrology of the Oklawaha River region should include some mention of the numerous springs along the river's course, especially between Eureka Bridge and Rodman Dam. Interviews with the "old-timers" of the region unleash countless stories of the delights of the small springs. Some of these springs can still be found bub-, bling from limestone orifices rimmed with white sand. Typically there would be a circular pool of gently swirling water drained by a short crystal brook running into the river:

Although there have been a number of investigations of the springs of Florida, there has not been work done specifically on these small beautiful springs of the Oklawaha.

It can be assumed that man has long found a certain fascination in springs. Not only have they served as needed sources of water, they have also been places of rest, worship, and healing. The event of appearing water, usually pristine, surely seemed to be almost magic -or at least the product of mysterious or miraculous circumstances. There is some evidence that the Indians of Florida utilized the springs as well as did the early settlers. However, remoteness from transportation routes had kept these springs relatively isolated.

The several Oklawaha springs do not serve as examples of springs of the first magnitude -- the "Big Springs" of the United States.

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Rather they are quiet pools, reflecting the myriad colors of the sub-tropical environment. The sylvan biome of the Oklawaha is a perfect setting for these crystal pools. The source of the water in these springs is, of course, ground water. Of all the water in the hydrologic cycle the part that sinks into the earth is termed "ground-water". Some is absorbed by the soil, some is used by plants, and some sinks by gravity deeper into the earth or rock. When this gravitational water reaches a fairly impermeable layer of material, it accumulates as a reservoir, the surface of which is called the "water table".

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The elevation of the water table in central Florida usually corresponds rather closely with the undulation of the topography, lying in smooth hills, ridges, depressions, and troughs. When the reservoir fills to overflowing, water moves through connected pore spaces, cracks, or other passageways. The flow is from higher to lower levels, down the hydraulic gradient or "slope" of the water table.

In some locations a permeable layer or aquifer is overlain by a less permeable stratum which may be termed an aquitard, or aquiclude. Water thus confined is said to be under artesian pressure and will sometimes flow out onto the surface without pumping. Thus, the ground-water reservoir may be classified as a water-table aquifer, or an artesian aquifer. These conditions give rise to the two kinds of springs found in Florida. Where the water table intersects with the land surface, there will be a seep, or spring. This water

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originally has fallen as rain and has percolated through the soil to the vater table. There it may move down-slope toward an outlet where it may be discharged. The other general type of spring is the flow from a confined aquifer issuing wherever the layer under pressure is exposed. This artesian water may come from great depths where it has been accumulating for many many years. Springs of this kind will yield a fairly steady flow and be only a little affected by variations in precipitation.

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Springs of both kinds sometimes discharge directly into stream beds, lakes, or river swamps, thus augmenting the surface waters. In times of flooding or high water, the flow of these springs, as well as that of those located nearby, may be reversed and the intake becomes a recharge for the aquifer. Thus the run-off or surface flow could enter the aquifer through the spring orifice.

The twenty springs along the Oklahawa described here were observed in an area reaching from Euraka Landing to Rodman. (See map.) About half were personally investigated, and the rest were described specifically and were located on air photographs by persons who have known the area well for many years.

In addition to the twenty "confirmed" springs, there are considered to be a number of others in the general area. Reliable sources vouch for their presence along the east or right bank north of Eureka.

The physiography of the area is most marked by the striking right-angle bend in the river near the mouth of Grange Creek.

...

Arralyses of the structure and geology of the underlying rocks show extensive jointing and some major faults. The springs may reflect the exposure by faulting of an older stratum, a portion of the regional aquifer.

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In the southernmost section of the part of the river under discussion here, there is a marked difference in the east and west bank topography. To the west lies the Oklawaha Lowlands, an extensive region of flatwoods underlain by clay deposits. This poorly drained ... land merges into the River Swamp immediately adjacent to the river itself. If springs arise in this swampy terrain, they are not readily discernable even from air photographs. They could more accurately be termed "seeps" for they could mark the areas where the ground level intersects the local water table.

The east, or right bank, is generally higher in elevation than the west and is much more easily studied. This area is designated physiographically as the Mount Dora Ridge, named for its more southerly extent. The region is chiefly comprised of the Fort Preston (or Hawthorn) formation of Miocene Age, which is generally send hills with lenses of gravel or clay. There are scattered deposits of pinkish-orange sendy clay of the Citronelle, as well as coarse send and gravel, possibly even Pliocene in age. These highlands are generally quite permeable and there is no major surface drainage other then the Oklawaha River itself. The response of the vegetation to the scarcity of available water is that of a "scrub-complex" with turkey cak in stands alternating with send pine. The gopher mouse, or

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"sandy mounder", leaves scattered spots of yellowish sand among the inhospitable scrub.

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Close to the river the slope of the ridge is covered with a hamock-type forest of hardwoods merging into the cypress of the river swamp. At many locations, the steep bank is quite close to the channel, offering good firm access to the main stream. Where the slope is of intermediate steepness and of moderate extent seems to be the favored locale of the small springs.

Springs in general may be classified into different types dependent upon their geologic occurrence, temperature, amount of water discharged, or the forces causing the springs. The small Oklawaha springs are limestone springs, mostly cold; possibly selt or sulfur; and usually artesian, but may be gravity-flow. The underlying water table, or the surface of the reservoir of ground water called the aquifer, is the Eocene Limestone exposed by the "levelling" of the structure of the Ocala Arch. As stated before, this water-table surface is seldom, if ever, flat; it undulates gently following the slope of the land. Where the overlying hills contain lenses of clay, there may be small local reservoirs, or "perched" ground water held above an aquitard. Water flowing from this perched stratum would be a gravity-flow spring and would diminish in volume during times of drought. The perennial flow from the Oklawaha indicates that most are powered by hydrostatic pressures built up in the regional aquifer.

Artesian flow-wells exist in the area, some known to carry water several feet above ground level. Also, distinctive limestone rocks can be dentified as late Eccene outcrops in several of the springs. So it seems likely that most of the springs of the east bank of the Oklawaha are representative of the Floridian aquifer.

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The several springs as numbered on the map are all changed to a greater or lesser degree by the elevation of the waters of the Rodman Pool. The lower locations are flooded and only faint outlines remain as evidence today. The somewhat higher springs are altered but are still present.

Blue Spring, No. 1, is located south of the river and is now inundated by the waters of the Rodman Reservoir. The large outline of the spring pool and run can be seen today. Only the rooftop remains of the spring-house. Tucked close between the high bluff and the river, the spring was perfect for those wishing to "get away from it all". It was privately owned for many years, but was always open for public use -- swimming and fishing, as well as picniding and camping. The most discriminating of seasoned fishermen marveled at the "quality" of fish of Blue Springs -- not to mention the quantity. Freshwater mullet and catfish swam like giant denizens convoyed by nervous bream, but the large bass was the most sought-after catch.

Roads of "ball-bearing" sand dusted with orange clay lead down and around the bluff to the relict Blue Springs. Tangles of muscadine and a few wild roses mark the way out to the low promontory. The oval outline of the spring-pool is marked by stark dead trees. The run is outlined by cypress skeletons on one side and the hardwood harmock trees on the other. Gone is the blue crystal pool and the jet-mirror stream, replaced by dead vegetation and murky water. The spring run was formerly long enough to merit the name of Indian Creek. Inother spring, unnamed and much smaller than Blue Spring, also feeds from the foot of the bluff into Indian Creek. (Shown by X on map.)

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Bright Angel Springs, north of the River, had two runs, both about the same size. One emptied into Horseshoe Creek which arched to the torth before joining the river. The other was very short and followed a direct route. Because of a huge cypress log in the water, this pool was sometimes called Log Springs. It was a favorite camping site. Between Bright Angel and Cedar Landing was a large turbulent spring welled with cabbage palm logs. This was Catfish Springs, comparable in volume with Blue Spring. Huge fish like black torpedoes would circle the boil. There were also mullet and striped bass in the turbulent water. There was a small spring only about twenty-five feet in circumference at Cedar Landing. It was easily possible to walk all the way around this one, stepping over the narrow run.

Near Agnew's Landing, upriver from Cecar Landing was an unnamed spring, No. 5 on the map. This spring was located almost in the river itself and was often flooded by high water. It was located between two huge cypress trees at the river's edge. When fishermen passed by at night, or during "nigh water", they could discern its location by its distinctive smell! No. 6 on the map represents a cluster of boils at the confluence of two creeks close to where they emptied into the river. The rocky springs made an unusually wide main trunk of Therman Creek. This stream was the location of a saw mill whose boilers remained at the site until only a few years ago. Sim's Spring flows out of a cleft in the rocky hillside below high land belonging to George Alcorn. This spring was developed many years ago and water was pumped to the top of the bluff by a steam pump. It was used for irrigation of an orange grove. This spring, protected by a coffer dam, is present today.

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No. 8 marks a "large" spring with a circular pool described also as being "between Sim's and Bud Springs". No. 9 is Bud Springs, not too far downstream from the Orange Creek Ferry site. This spring had a large deep pool with the water spilling over a shelf and spreading into a wide shallow run to the river.

Existing today are Mullet Cove Spring, Indian Bluff Spring, and a small spring at Tobacco Patch Landing. Cannon Springs, Numbers 13-18, are found at Couse Landing between Tobacco Patch Landing and Eureka. Signs call them "Sparks Springs", but the old name more often used is Cannon. There are at least six springs of varying sizes remaining. They are arranged in a rough line forming a slough resembling a meander cutoff in the river. Several different kinds of fish can be seen today in the largest pool, as well as a variety of birds. (The manhinga dries its wings, wet from fishing.) The forest here is perhaps the most beautiful of all that along the river. It is a low-hammock type with a mixture of palms and hardwoods. The cry of the limpkin is a noisy and interesting distraction in the quiet woods.

Several small springs are reported near the farm of Elmer Fiddia, upriver from Cannon Springs. Also there is at least one more spring, nearer Eureka than the rest. This one is called Dudley Spring, named For its most recent owner. It is reported to be near in size to the largest of the Cannon Springs pools.

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Not included specifically, but indicated by X's on the map, are some of the springs near Orange Creek. The principal one is Orange Springs itself, a sulfur spring west of the mouth of the Creek. It is a walled-in roughly circular pool about 75 feet across. The boil is about eighteen feet deep; but, except for this area, the water is shallow. The run into Orange Creek is about 500 feet long. The sulfur is said to be organic in origin, the hydrogen sulfide from ancient decayed vegetation. Another "spring" nearby is Seminole Spring, a man-made flow from artesian wells drilled into two small springs near Orange Creek. Among the numerous small springs, some only drinking springs, are Maria Spring and White Spring. Also there is a "drilled" spring in Collin's Slough between the McRae farm and the Oklawaha River. The artesian well nearby has existed for decades and has been used regularly for data-recording by the Geological Survey.

The springs of the middle Oklawsha do certainly contribute to the. volume of the river. All together, however, they do not amount to as much as that from Silver Springs Run, a combined flow from fourteen spring complexes. On the average, nevertheless, the river increases in volume by almost one-third when measured between gauges at Conner (just below Eureka) and at Riverside (below Orange Ferry). If the flow of Orange Creek is subtracted, the increase in volume must be from the several springs along the river. Clean, unpolluted water from these springs no doubt also adds to the overall quality of the river water.

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Almost all of these springs have been damaged or destroyed by man and are not flowing  $\frac{1}{2}$ , their maximum tiped. No doubt some are beyond salvage, but certainly a few could be we stored and preserved to contribute to the net wit, beauty of the *Matic* net Firest

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<u>No.</u>	Name	Location	Approximate Dimensions	Run	Comments	Existing Today	
1	Blue Spring	South of river Near Dutchman's Reach	200' N-S 350' E-W 22' deep	5 miles long (Indian Creek) 40' wide - 6' deep	Largest of these springs, spring- house, landscaping	No	
2	Bright Angel (or Log) Spring	North of river almost opposite Catfish Spring	Round pool 30' diam. 25' deep	2 runs 8' wide 2' deep 1-into river 2-into Horse- shoe creek	Cypress log in water	No	
3	Catfish Spring	South of river below Cedar Land- ing	Round pool 50' diam.	100' long 30' wide	Large volume, turbulent flow, once walled with cabbage-palm logs	No	
4	Cedar Landing Spring	South of river at Cedar Landing	Round pool 8' diam,	150' long	Small spring	No	
5		On bank, directly on river near Agnew's Landing	No pool, just orl- fice	llo run	Directly on edge of river, sometimes flooded	No	
6	(cluster)	At confluence of Therman Greek and another stream	Cluster of several boils in rocky con- fluence	No tun, creek empties di- rectly into river	Therman Greek parallels river as far as Blue Springs saw mill site	No	
7	Sim's Spring	At George'AL- corn's out of cleft in rock bluff	No pool, flow di- rectly out of hill face	No data	Protected by coffer dam, once pumped to top of hill	Yes	
		· · · ·	•				

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	a a constant a sub-	Location	D' isions	Run	Common i	Exis	· · ·
8		Large spring be- tween Sim's and Bud Spring	"Large" pool	No data	Strong flow	Tot. : No	•
9	Bud Spring	East of river, nearly opposite mouth of Orange Creek	Round pool 35' diam.	650' long 50' wide 3' deep	Appeared to come straight up, then emptied over shelf into shallow run	No	
10	Fullet Cove Spring	East bank, close to Wells Landing	2 small boils	No data	No data	Yes	
. 11	Indian Bluff Spring	East bank, above Tobacco Patch Landing	No data	No data	Clear water flowing out of swamp	Yes	· · ·
1.2		East bank at Tobacco Patch Landing	No data	No data	Small spring	Yes	12 -
1.3-13	B Caupon (or Sugar		•				:
	Spring	East bank, scv- cral pools in a line	Round pool 50' diam.	200', in slough	At least 3 large and 3 small springs	Yes	•
19		East bank, near mouth of Mill Creek	No data	No data	At Elmer Fiddia's	Yes	:
20	Dudley Spring	East Bank, nearest Eureka	No data	No data	Dudley, last owner	Yes	
							:
	4						

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#### SOURCES USED

Air Photos, 1940, 1943, and 1949, Geography Department, University of Florida.

Allen, Ross, 1971, Personal interview, Silver Springs, Florida.

Bielling, Paul, 1971, Personal interviews and field trip, Fort McCoy, Florida.

Blassingame, Wyatt, 1966, Goodbye Blue Springs: Field and Stream, "' February, 1966.

Chapman, Donald V., 1971, Parsonal interviews, Orange Springs, Florida.

- Faulkner, G. L., 1970. Geohydrology of the Cross-Florida Barge Canal with special Reference to the Ocala vicinity: United States Geological Survey Open File Report, Tallahassee, Florida.
- Ferguson, G. E., C. W. Lingham, S. K. Love, and R. O. Vernon, 1947, Springs of Florida: Florida Geological Survey Bull. No. 31, Tallahassee, Florida.
- Florida Defenders of the Environment, 1970, Environmental Impact of the Cross-Florida Barge Canal with special emphasis on the Oklawaha Regional Ecosystem, Gainesville, Florida.

Johnson, Ruby, 1971, Personal interview, Orange Springs, Florida.

Taylor, G. H., after 1959, Springs their Origin, Development, and Protection: United States Geological Survey.

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## **APPENDIX III**

## **Discharge reports**

Blue Spring, Marion County, 9-07 Discharge Report Bright Angel Spring, 9-07 Discharge Report Fish Hook #1 spring, 9-07 Discharge Report Catfish Convention Hall Spring, 9-07 Discharge Report Lost River Spring, 9-07 Discharge Report Mammoth Spring, 9-07 Discharge Report Discharge Measurement: Blue Spring, Rodman Reservoir/Ocklawaha River, Marion County, Florida; September 27, 2007

Prepared for: **St. Johns River Water Management District** 4049 Reid Street Palatka, Florida 32177

Prepared by: **Karst Environmental Services, Inc.** 5779 NE County Road 340 High Springs, Florida 32643 (386) 454-3556 (386) 454-3541 FAX

kes@atlantic.net

# Discharge Measurement: Blue Spring, Marion County, Florida; September 27, 2007

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- 2. Table 1. Discharge of Blue Spring, Marion County, Florida on September 27, 2007. Data record and calculation of discharge measurement.
- 3. Figure 1A. Underwater video still of Blue Spring (Marion County). View of the upper vent measurement cross-section.
- 4. Figure 1B. Underwater video still of Blue Spring (Marion County). View of the lower vent.
- 5. Figure 2. Discharge measurement cross-section; Blue Spring, Marion County, Florida, September 27, 2007 measurement.
- 6. Figure 3. Discharge measurement cross-section; Blue Spring, Marion County, Florida, September 27, 2007 measurement. Flow contour velocities are shown ...
- 7. Table 2. Blue Spring (Marion County), September 27, 2007. Surfer 8 Grid Volume Computations and Gridding Report.
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# Results of Discharge Measurements of Blue Spring, Marion County, Florida; September 27, 2007

## **INTRODUCTION**

The St. Johns River Water Management District (SJRWMD) contracted with Karst Environmental Services, Inc. (KES) to perform discharge measurements of selected submerged springs that discharge into the Rodman Reservoir/Ocklawaha River in Marion and Putnam Counties, Florida. This report documents the results of the measurement made at the Blue Spring (Marion County) site on September 27, 2007. A summary of the results and collected data for that measurement are presented on Table 1.

## PURPOSE and SCOPE OF WORK

The purpose of this work was to obtain an initial discharge measurement of Blue Spring (Marion County), which is among the many sources of groundwater discharging into the Rodman Reservoir/Ocklawaha River. A program of discharge measurements was to be made of the springs in the Rodman Reservoir/Ocklawaha River during September of 2007.

#### SITE DESCRIPTION

Blue Spring (Marion County) is located on the south side of the Rodman Reservoir and the Ocklawaha River channel, southeast of the public boat ramp at Kenwood Landing, at 416958 Easting/3265285 Northing (UTM Zone 17, NAD 1983 HARN, meters), or Lat. N29.514404°, Long. W81.856850° (WGS84).

The spring discharges primarily from two vents in bedrock, at the bottom of a large basin. The upper and larger vent was about 31 feet deep (during this measurement), and a lower vent was at about 33 feet deep. The vents are too small to allow for diver entry, and conditions around them during this measurement were very silty. See Figures 1A and 1B. There was considerable aquatic vegetation present in the spring basin area.

Since the vents of this spring are located on the bottom of the river, its discharge cannot be measured by conventional discharge measurement methods. However, the upper spring vent opening provided a suitable location for a discharge measurement that lends itself to the application of an appropriately adapted instrument.

#### PERSONNEL

Fieldwork for this discharge measurement was conducted by KES personnel Peter Butt and Tom Morris. Jeff Davis of the SJRWMD was also on site during the measurement, and provided logistics support. Data management and report preparation was performed by Peter Butt. Data processing using Surfer 8 contouring software was performed by W. Bruce Lafrenz, P.G., of Tetra Tech of Orlando, Florida.

## **METHODS**

#### Instrumentation

The instrument used for this discharge measurement was a Marsh-McBirney Model 2000 Flo-Mate electronic flowmeter (Serial Number 2002679) that has been adapted for fully submersible use. In order to operate and read the meter at depth, the unit has been placed within an underwater housing with a transparent lid. The sensor wire is routed through a sealing gland on the housing lid. There are two housing controls that allow for direct operation of the flow meter. One operates the on/off/reset buttons, and the other operates the time interval selector buttons that control the measurement period.

The flowmeter used was factory calibrated while in its underwater housing in the method normally used for this unit on April 20, 2007. A copy of the Calibration Certificate is included with this report.

A video record of the site was made on August 29, 2007.

#### Field Operations

Velocity measurements were taken at the upper-most vent. The measurement site was 31 feet deep. Cross-section dimensions were approximately 5 feet long by 2 feet wide. A lower vent was blocked with plastic bubble wrap sheets to eliminate open areas that could not be measured.

Four telescoping aluminum poles with 0.1, 0.25, 0.5 and one-foot interval markings were positioned horizontally to provide a positioning grid for velocity measurements. As all sensor-support poles were positioned at right angles to the main flow path, no angle coefficient corrections for velocity readings were made. The flowmeter sensor was positioned on the poles with a low-profile metal spring clamp. Conduit dimensions around the grid were measured with a collapsible steel tape. See Figure 2.

Peter Butt positioned the sensor and recorded positional data, while Tom Morris took the velocity readings after taking reset cues from Butt. During all measurements, the sensor handler was able to move away from the measurement cross-section, and remove himself from the cross section of the flow. The meter operator was also positioned above and away from the cross-section. This minimized or eliminated the possibility of interference with flow while the measurements were taken. The flowmeter was operated in the "Fixed Point Averaging" mode. Fixed Point Averaging is an average of velocities over a fixed period of time. Averaging periods of 60 seconds were used. The flowmeter was reset between each station. Twenty-one station readings were made.

#### Data Processing

Field measurements of the velocity measurement stations and vent boundaries were plotted on grid paper and assigned X- and Y-axis values. See Figure 2. Values for the Z-axis were the point velocities, and zero values were assigned to the cross-section boundary points. See Table 3. The X, Y and Z data was processed using the Surfer v.8 (by Golden Software, Inc.) contouring program. The gridding method used was point Kriging with linear drift, and anisotropy ratio of 1 at an angle of  $0^{\circ}$ , and a variogram slope of 1. The results of the contour processing are illustrated in Figures 3 and 4.

Discharge and measurement cross-section area are given on the Grid Volume Computations and Gridding Report feature of the software, included in this report on page 1 of Table 2. The total discharge is shown as the "**Net Volume (Cut-Fill)**". The Net Volume value is used because a Surfer 8 "blanking file" operation was used to define the measurement cross-section boundary and eliminate artifacts present in the contouring process that would create inaccuracies in the flow calculations. The software also calculated the total cross-sectional area of the measurement location within the passage, and is shown in square feet as the "**Positive Planar Area (Cut)**".

#### **RESULTS AND DISCUSSION**

This measurement is the first one performed at Blue Spring (Marion County) applying the method and data processing used at other spring sites by KES. Based on KES' experience at other springs, the estimate of discharge for this initial measurement should be considered to be a minimum value. The data from this measurement will also provide a guide for the planning and improvements for any future measurements of this type here.

The estimated discharge of Blue Spring (Marion County) on September 27, 2007 was 0.778 CFS (cubic feet per second). This result is also expressed as 349 GPM (gallons per minute) or 0.503 MGD (million gallons per day), see Table 1. Twenty-one (21) readings were made, see Figures 2 and 4. The point velocity readings ranged from 0 to 0.66 feet per second (fps), with an overall average station reading of 0.30 fps. The total cross-sectional area was calculated as 4.42 square feet. Individual point velocity measurement periods of 60 seconds were used. The measurements commenced at about 11:44 hours and were completed by 12:18.

UNDERWATER DISCHARGE MEASUREMENT				
Location:	BLUE SPRING (MARION COUNTY)		Date:	September 27, 2007
	Rodman Reservoir/Ocklawaha River		Time Start:	11:44
	Marion County, Florida		Time End:	12:18
Personnel:	Peter Butt, Tom Morris			
Method:	Grid within irregular c	onduit		
Instrument:	MMB2000 FLO-MATE	E in U/W case, sensor or	n support poles	
Analysis Method	: Surfer 8 with kriging	1		
 Dius Caring /	Varian County) Tate			
Blue Spring (I		a Discharge.		
	0.776			
	0.505			
Grivi Total Cross so	stional Area:	4.42	cauaro foot	
Avg Station B	cional Alea.	4.42	foot/cocond	
Avg. Station F	Dinit Velocity.	0.30	feet doop	
Memt Periode		31 60 soconds	leet deep	
Volocity Poodi	na hy Station:	(All velocity reading	in foot por soo	and )
 velocity Reading by Station:			s in leet per seu	
Station #	Point Velocity			
1	0.23			
2	0.39			
3	0.48			
4	0.31			
5	0.12			
6	0.03			
7	0.02			
8	0.54			
9	0.54			
10	0.06			
11	0.53			
12	0.64			
13	0.38			
14	0.01			
15	0.04			
16	0.01			
17	0			
18	0.49			
19	0.66			
20	0.62			
21	0.13			

Table 1. Discharge of Blue Spring, Marion County, Florida on September 27, 2007. Data record and calculation of discharge measurement.



Figure 1A. Underwater video still of Blue Spring (Marion County). View of the upper vent measurement cross-section.



Figure 1B. Underwater video still of Blue Spring (Marion County). View of the lower vent.



Figure 2. Discharge measurement cross-section; Blue Spring, Marion County, Florida, September 27, 2007 measurement. Cross-section is viewed to the upstream of observer, and is located at the 31-foot depth level. Velocity measurement stations are shown as numbered points. See Table 1 for station velocities. Boundary of cross section is shown as connected, lettered points. Support poles represented by dashed lines. X- and Y-axis scales are shown in feet.



Figure 3. Discharge measurement cross-section; Blue Spring, Marion County, Florida, September 27, 2007 measurement. Flow contour velocities are shown in feet per second. Outer boundary of cross section represents the zero-value contour. X-and Y-axis scales are shown in feet.

# TABLE 2. BLUE SPRING, MARION COUNTY, SEPTEMBER 27, 2007.SURFER 8 GRID VOLUME COMPUTATIONS AND GRIDDING REPORT

## **UPPER SURFACE**

Grid File Name:	Y:\2. PROJECTS\KARST ENVIRONMENTAL\Rodman\Oklawaha
	Blue\2007-09\OklawahaBlue_09-2007.bln.grd
Grid Size:	61 rows x 121 columns
X Minimum:	0
X Maximum:	6
X Spacing:	0.05
Y Minimum:	0
Y Maximum:	3
Y Spacing:	0.05
Z Minimum:	-1.5712924850142E-009
Z Maximum:	0.68867191012325

## LOWER SURFACE

Level Surface defined by Z = 0

#### VOLUMES

Z Scale Factor:	1
Total Volumes by:	
Trapezoidal Rule:	0.7776379372613
Simpson's Rule:	0.77745177168607
Simpson's 3/8 Rule:	0.77755008943736

#### **CUT & FILL VOLUMES**

Positive Volume [Cut]:0.77763793728787Negative Volume [Fil]:2.6577153317253E-011Net Volume [Cut-Fil]:0.7776379372613<<<<<<Total Discharge in CFS</th>(The Net Volume value is used due to the use of a blanking file operation in the calculations.Positive Vol. Cut - Negative Vol. Fill = Net Volume. Please refer to report text.)

# AREAS

Planar Areas	
Positive Planar Area [Cut]:	4.4187497474909<<< <cross-section feet<="" in="" square="" th=""></cross-section>
Negative Planar Area [Fill]:	2.5250913671836E-007
Blanked Planar Area:	13.58125
Total Planar Area:	18
~ ^ /	

#### **Surface Areas**

Positive Surface Area [Cut]:	5.7080588704276
Negative Surface Area [Fill]:	2.526421860012E-007

# **GRIDDING REPORT**

## **Data Source**

Source Data File Name:	Y:\2. PROJECTS\KARST ENVIRONMENTAL\Silver Springs\Sep 07\Rodman\OklawahaBlue\Oklawaha Blue 9-07 SURFER XYZ
	T3BLF.xls
X Column:	A
Y Column:	В
Z Column:	С
Data Counts	
Active Data:	258
Original Data:	258
Excluded Data:	0
Deleted Duplicates:	0
Retained Duplicates:	0
Artificial Data:	0
Superseded Data:	0

# **Univariate Statistics**

	Х	Y	Z
Minimum:	0.1	0.5	0
25%-tile:	1.6665	1.4	0
Median:	3.2	1.95	0
75%-tile:	4.5	2.24442	0
Maximum:	5.6	2.7	0.66
Midrange:	2.85	1.6	0.33
Range:	5.5	2.2	0.66
Interquartile Range:	2.8335	0.84442	0
Median Abs. Deviation:	1.35	0.45	0
Mean:	3.0501821705426	1.7745624418605	0.024147286821705
Trim Mean (10%):	3.0683632478632	1.7915983333333	0.0017948717948718
Standard Deviation:	1.5942309741642	0.57103042152364	0.10597027525125
Variance:	2.5415723989844	0.32607574230547	0.011229699236825
Coef. of Variation:			4.3884961500516
Coef. of Skewness:			4.6474890629164

# **Inter-Variable Correlation**

	Х	Y	Z	
X:	1.000	-0.446	0.121	
Y:		1.000	0.040	
Z:			1.000	

Table 2. Blue Spring (Marion County), September 27, 2007.

### **Inter-Variable Covariance**

	Х	Y	Z
X: Y: Z:	2.5415723989844	-0.40570835827429 0.32607574230547	0.020485911153176 0.0024456433612764 0.011229699236825

# **Planar Regression: Z** = **AX**+**BY**+**C**

## **Fitted Parameters**

	А	В	С
Parameter Value:	0.011551945730664	0.021873336078634	-0.049903852764376
Standard Error:	0.0045894137435241	0.0128129522831	0.032242000829751

# **Inter-Parameter Correlations**

	А	В	С
A: B: C:	1.000	-0.446 1.000	-0.748 0.899 1.000

# **ANOVA Table**

Source	df	Sum of Squares Mean Square F
Regression:	2	0.074857800368025 0.037428900184013 3.3816
Residual:	255	2.8224046027327 0.01106825334405
Total:	257	2.8972624031008

Coefficient of Multiple Determination (R^2): 0.025837425111343

# **Nearest Neighbor Statistics**

	Separation	Delta Z
Minimum:	0.02222	0
25%-tile:	0.050249378105604	0
Median:	0.053851648071345	0
75%-tile:	0.058309518948453	0
Maximum:	0.34409301068171	0.64

Midrange:	0.18315650534085 0.32
Range:	0.32187301068171 0.64
Interquartile Range:	0.0080601408428484 0
Median Abs. Deviation:	0.0038516480713451 0
Mean:	0.067863270217325 0.015348837209302
Trim Mean (10%):	0.059103331013652 0.001025641025641
Standard Deviation:	0.048694669457837 0.07715429533957
Variance:	0.002371170833608 0.0059527852893456
Coef. of Variation:	0.7175408627067 5.0267192418205
Coef. of Skewness:	3.4942043561896 6.2296297163987
Root Mean Square:	0.083526009591011 0.078666206804595
Mean Square:	0.0069765942781977 0.0061883720930233

# **Complete Spatial Randomness**

Lambda:	21.322314049587
Clark and Evans:	0.62673211188472
Skellam:	241.14450909942

# **Exclusion Filtering**

Exclusion Filter String: Not In Use

# **Duplicate Filtering**

Duplicate Points to Keep:	First
X Duplicate Tolerance:	6.5E-007
Y Duplicate Tolerance:	2.6E-007
No duplicate data were fou	ınd.

## **Breakline Filtering**

Breakline Filtering: Not In Use

# **Gridding Rules**

Gridding Method:	Kriging
Kriging Type:	Point
Polynomial Drift Order:	1
Kriging std. deviation grid:	no

## **Semi-Variogram Model**

Component Type:	Linear
Anisotropy Angle:	0
Anisotropy Ratio:	1
Variogram Slope:	1

# **Search Parameters**

No Search (use all data): true

# **Output Grid**

Grid File Name:	Y:\2. PROJECTS\KARST ENVIRONMENTAL\Silver Springs\Sep 07\Rodman\OklawahaBlue\OklawahaBlue_9-07.grd
Grid Size:	61 rows x 121 columns
Total Nodes:	7381
Filled Nodes:	7381
Blanked Nodes:	0
Grid Geometry	
X Minimum:	0
X Maximum:	6
X Spacing:	0.05
Y Minimum:	0
Y Maximum:	3
Y Spacing:	0.05
Grid Statistics	
Z Minimum:	-0.32931531856656
Z 25%-tile:	-0.093850815718461
Z Median:	-0.013977374731127
Z 75%-tile:	0.011834200593412
Z Maximum:	0.68867191012325
Z Midrange:	0.17967829577835
Z Range:	1.0179872286898
Z Interguartile Range:	0.10568501631187
Z Median Abs. Deviation:	0.04253545003506
Z Mean:	-0.010212294742361
Z Trim Mean (10%):	-0.026274626095364
Z Standard Deviation:	0.16162503137099
Z Variance:	0.026122650765674
Z Coef. of Variation:	-1
Z Coef. of Skewness:	1.868114795289
Z Root Mean Square:	0.16194734245914
Z Mean Square:	0.026226941729579



Figure 4. Discharge measurement cross-section; Blue Spring, Marion County, Florida, September 27, 2007 measurement. Relationship of flow contours (velocities shown in feet per second) and velocity measurement stations (numbered points) are shown. See Table 1 for station velocities. Boundary of cross section is shown as connected, lettered points. X- and Y-axis scales are shown in feet.

Table 3. Blue Spring (Marion County) XYZ Grid Data September 27, 2007.					
v	v	7 (Valaaity)	Station #	V Plot	V Plot
A	1				1 10
4.0	2 25	0.23		90	40
4.5	2.25	0.39	2	90	40
4.5	1 75	0.40	3	90	40
4.5	1.75	0.31	4	90	30
4.5	1.5	0.12	5	90	30
4.5	1.25	0.03	7	90	20
4.5	2 25	0.02	7	90	47
4.1	1.85	0.54	0	82	37
4.1	1.05	0.04		82	27
4.1	1.55	0.00	10	80	40
35	2	0.55	12	70	40
3.5	2	0.04	12	60	40
25	2	0.50	14	50	40
2.5	2	0.01	14	40	40
1.5	2	0.04	16	30	40
1.5	2	0.01	17	20	40
3 85	16	0.49	17	77	32
3.05	1.0	0.49	10	72	32
3.0	1.0	0.00	20	62	32
1.85	1.0	0.02	20	97	32
4.00	1.0	0.10	21	57	52
0 1	2	0	Δ	2	40
0.7	2	0	B	14	40
1	1.9	0	C	20	38
1.5	1.75	0	D	30	35
1.75	1.45	0	E	35	29
2	1.45	0	F	40	29
2.25	1.4	0	G	45	28
2.5	1.5	0	Н	50	30
2.75	1.55	0	I	55	31
3	1.4	0	J	60	28
3.25	1.4	0	K	65	28
3.5	1.25	0	L	70	25
3.75	1.25	0	М	75	25
4	1.2	0	N	80	24
4.1	1.1	0	0	82	22
4.2	1	0	Р	84	20
4.5	0.5	0	Q	90	10
5.6	1	0	R	112	20
5.6	1.1	0	S	112	22
5.35	1.25	0	Т	107	25
5.2	1.5	0	U	104	30
5.05	1.75	0	V	101	35
5.1	1.85	0	W	102	37
5	2	0	X	100	40

Х	Y	Z (Velocity)	Station #	X Plot	Y Plot
4.7	2.25	0	Y	94	45
4.7	2.35	0	Z	94	47
4.5	2.55	0	AA	90	51
4.3	2.55	0	BB	86	51
4.1	2.7	0	CC	82	54
4	2.7	0	DD	80	54
3.75	2.5	0	EE	75	50
3.65	2.35	0	FF	73	47
3.5	2.3	0	GG	70	46
3.25	2.2	0	HH	65	44
3	2.2	0	II	60	44
2.75	2.1	0	JJ	55	42
2.5	2.15	0	KK	50	43
2.25	2.25	0	LL	45	45
2	2.4	0	MM	40	48
1.75	2.45	0	NN	35	49
1.5	2.45	0	00	30	49
1	2.4	0	PP	20	48
0.15	2	0	A1	3	40
0.2	2	0	A2	4	40
0.25	2	0	A3	5	40
0.3	2	0	A4	6	40
0.35	2	0	A5	7	40
0.4	2	0	A6	8	40
0.45	2	0	A7	9	40
0.5	2	0	A8	10	40
0.55	2	0	A9	11	40
0.6	2	0	A10	12	40
0.65	2	0	A11	13	40
			<b></b>	45	00.07
0.75	1.9835	0	B1	15	39.67
0.8	1.967	0	B2	16	39.34
0.85	1.9505	0	B3	17	39.01
0.9	1.934	0	B4	18	38.68
0.95	1.9175	0	В5	19	38.35
4.05	4.005	•	01	01	07.7
1.05	1.885	U		21	31.1
1.1	1.87	0	C2	22	37.4
1.15	1.855	0		23	37.1
1.2	1.84	0		24	30.8 26.5
1.25	1.823	0		20	30.5
1.3	1.01	0		20	30.2
1.35	1./95	0		21	35.9
1.4	1./8	U		28	33.0 25.0
1.45	1./00		C9	29	33.3
4 5 4 4 5	4 7	^		20.02	24
1.5415	1.7	U	וע	30.83	34

X	Y	Z (Velocity)	Station #	X Plot	Y Plot
1.583	1.65	0	D2	31.66	33
1.6245	1.6	0	D3	32.49	32
1.6665	1.55	0	D4	33.33	31
1.7075	1.5	0	D5	34.15	30
1.8	1.45	0	E1	36	29
1.85	1.45	0	E2	37	29
1.9	1.45	0	E3	38	29
1.95	1.45	0	E4	39	29
2.05	1.44	0	F1	41	28.8
2.1	1.43	0	F2	42	28.6
2.15	1.42	0	F3	43	28.4
2.2	1.41	0	F4	44	28.2
2.3	1.42	0	G1	46	28.4
2.35	1.44	0	G2	47	28.8
2.4	1.46	0	G3	48	29.2
2.45	1.48	0	G4	49	29.6
	0				
2.55	1.51	0	H1	51	30.2
2.6	1.52	0	H2	52	30.4
2.65	1.53	0	H3	53	30.6
2.7	1.54	0	H4	54	30.8
2.0	4.50	0	14	56	20.4
2.8	1.52	0		57	30.4
2.05	1.49	0	12	58	29.0
2.5	1.40	0	13	50	29.2
2.95	1.45	0	14		20.0
3 05	14	0	.l1	61	28
3.1	1.4	0	J2	62	28
3.15	1.4	0	J3	63	28
3.2	1.4	0	J4	64	28
3.3	1.37	0	K1	66	27.4
3.35	1.34	0	K2	67	26.8
3.4	1.31	0	K3	68	26.2
3.45	1.28	0	K4	69	25.6
3.55	1.25	0	L1	71	25
3.6	1.25	0	L2	72	25
3.65	1.25	0	L3	73	25
3.7	1.25	0	L4	74	25
3.8	1.24	0	M1	76	24.8
3.85	1.23	0	M2	77	24.6
3.9	1.22	0	M3	78	24.4

X	Y	Z (Velocity)	Station #	X Plot	Y Plot
3.95	1.21	0	M4	79	24.2
4.05	1.15	0	N1	81	23
4.15	1.05	0	01	83	21
4.23	0.95	0	P1	84.6	19
4.26	0.9	0	P2	85.2	18
4.29	0.85	0	P3	85.8	17
4.32	0.8	0	P4	86.4	16
4.35	0.75	0	P5	87	15
4.38	0.7	0	P6	87.6	14
4.41	0.65	0	P7	88.2	13
4.44	0.6	0	P8	88.8	12
4.47	0.55	0	P9	89.4	11
4.55	0.52273	0	Q1	91	10.4545
4.6	0.54545	0	Q2	92	10.909
4.65	0.56818	0	Q3	93	11.3635
4.7	0.5909	0	Q4	94	11.818
4.75	0.61363	0	Q5	95	12.2725
4.8	0.63635	0	Q6	96	12.727
4.85	0.65908	0	Q7	97	13.1815
4.9	0.6818	0	Q8	98	13.636
4.95	0.70453	0	Q9	99	14.0905
5	0.72725	0	Q10	100	14.545
5.05	0.74998	0	Q11	101	14.9995
5.1	0.7727	0	Q12	102	15.454
5.15	0.79543	0	Q13	103	15.9085
5.2	0.81815	0	Q14	104	16.363
5.25	0.84088	0	Q15	105	16.8175
5.3	0.8636	0	Q16	106	17.272
5.35	0.88633	0	Q17	107	17.7265
5.4	0.90905	0	Q18	108	18.181
5.45	0.93178	0	Q19	109	18.6355
5.5	0.9545	0	Q20	110	19.09
5.55	0.97723	U	Q21	111	19.5445
<b>.</b>	4.05		<b>D</b> 4	110	01
0.0	1.05	U	RI	112	21
5 55	1 1 2	0	<u>81</u>	111	22.6
5.55	1.13	0	<u> </u>	110	22.0
5.5	1.10	0	52 53	109	23.2
5 /	1.13	0	55 54	109	20.0
5.4	1.22	0	- 54	100	27.4
5 32	13	Λ	T1	106.4	26
5 29	1 35	0	T2	105.9	20
5.23	1.55	0	T2	105.0	28
5.20	1.4	5	13	100.2	20

X	Y	Z (Velocity)	Station #	X Plot	Y Plot
5.23	1.45	0	T4	104.6	29
5.17	1.55	0	U1	103.4	31
5.14	1.6	0	U2	102.8	32
5.11	1.65	0	U3	102.2	33
5.08	1.7	0	U4	101.6	34
5.075	1.8	0	V1	101.5	36
5.0665	1.9	0	W1	101.33	38
5.033	1.95	0	W2	100.66	39
4.95	2.04167	0	X1	99	40.8333
4.9	2.08333	0	X2	98	41.6666
4.85	2.125	0	X3	97	42.4999
4.8	2.16666	0	X4	96	43.3332
4.75	2.20833	0	X5	95	44.1665
4.7	2.3	0	Y1	94	46
4.65	2.4	0	Z1	93	48
4.6	2.45	0	Z2	92	49
4.55	2.5	0	Z4	91	50
4.45	2.55	0	AA1	89	51
4.4	2.55	0	AA2	88	51
4.35	2.55	0	AA3	87	51
4.25	2.5875	0	BB1	85	51.75
4.2	2.625	0	BB2	84	52.5
4.15	2.6625	0	BB3	83	53.25
1.05					<b>5</b> 4
4.05	2.7	0	CC1	81	54
2.05	22.0	0		70	52.2
3.95	2.00	0		79	53.2
3.9 2.95	2.02	0		70	51.6
3.00 2 0	2.30	0		76	50.9
3.0	2.34	U	004	70	50.6
3 7165	2 / 5	0	EE1	7/ 33	19
3.683	2.45	0	EE1	73.66	43
5.005	<u> </u>	U U		10.00	
3.6	2.3335	0	FF1	72	46 67
3 55	2 317	0	<b>FF</b> 2	71	46.34
0.00	2.011	<b>.</b>		· · ·	10.04
3.45	2.28	0	GG1	69	45.6
3.4	2.26	0	GG2	68	45.2
3.35	2.24	0	GG3	67	44.8
		-			

X	Y	Z (Velocity)	Station #	X Plot	Y Plot
3.3	2.22	0	GG4	66	44.4
3.2	2.2	0	HH1	64	44
3.15	2.2	0	HH2	63	44
3.1	2.2	0	HH3	62	44
3.05	2.2	0	HH4	61	44
2.95	2.18	0	ll1	59	43.6
2.9	2.16	0	ll2	58	43.2
2.85	2.14	0	ll3	57	42.8
2.8	2.12	0	114	56	42.4
	0				
2.7	2.11	0	JJ1	54	42.2
2.65	2.12	0	JJ2	53	42.4
2.6	2.13	0	JJ3	52	42.6
2.55	2.14	0	JJ4	51	42.8
2.45	2.17	0	KK1	49	43.4
2.4	2.19	0	KK2	48	43.8
2.35	2.21	0	KK3	47	44.2
2.3	2.23	0	KK4	46	44.6
2.2	2.28	0	LL1	44	45.6
2.15	2.31	0	LL2	43	46.2
2.1	2.34	0	LL3	42	46.8
2.05	2.37	0	LL4	41	47.4
					10.0
1.95	2.41	0	MM1	39	48.2
1.9	2.42	0	MM2	38	48.4
1.85	2.43	0	MM3	37	48.6
1.8	2.44	0	MINI4	36	48.8
47	2.45	0		24	40
1.7	2.45	0		34	49
1.05	2.45	0	NN2	32	49
1.0	2.45	0		31	49
1.55	2.45	0	ININ4	51	43
1 /5	2 1 1 5	0	001	20	18.9
1.45	2.445	0	002	23	48.8
1 35	2.44	0	003	20	48.7
1.00	2 43	0	004	26	48.6
1.25	2.425	0	005	25	48.5
1.2	2.42	0	006	24	48.4
1.15	2.415	0	007	23	48.3
1.1	2.41	0	008	22	48.2
1.05	2.405	0	009	21	48.1
		-		· ·	
0.95	2.37774	0	PP1	19	47.5548
l	1		1	1	1

X	Y	Z (Velocity)	Station #	X Plot	Y Plot
0.9	2.35552	0	PP2	18	47.1104
0.85	2.3333	0	PP3	17	46.666
0.8	2.31108	0	PP4	16	46.2216
0.75	2.28886	0	PP5	15	45.7772
0.7	2.26664	0	PP6	14	45.3328
0.65	2.24442	0	PP7	13	44.8884
0.6	2.2222	0	PP8	12	44.444
0.55	2.19998	0	PP9	11	43.9996
0.5	2.17776	0	PP10	10	43.5552
0.45	2.15554	0	PP11	9	43.1108
0.4	2.13332	0	PP12	8	42.6664
0.35	2.1111	0	PP13	7	42.222
0.3	2.08888	0	PP14	6	41.7776
0.25	2.06666	0	PP15	5	41.3332
0.2	2.04444	0	PP16	4	40.8888
0.15	2.02222	0	PP17	3	40.4444

	CALIBRA	TION CERTIFIC	ATE
Model: 20	00	_Serial Number: 20	02679
Unit Gain Ratio	o:	Time Cons	tant:
	-	Type of Reading	
Velocity:	5	Level:	
		L	
		Ī	N/A
	Static Velocity	Dynamic Velocity	Level
Standard:	Zero	2.00	NA
Measured:	0.00	2.00	NA
Factory C Field Prof	alibration ile Calibration; ïcient or Velocity M	fultiplier:	•
Calibration Te QA Technician	chnician:	/	Date: <u>4-20-07</u> Date: <u>2014147</u>
This documen Verification is is traceable to Gaithersburg, the Customer	t certifies that the o indicated by the m the National Institu MD. For product in Service Department	described instrument ha easured results show a ute of Standards and T nformation, service, or o nt.	as been calibrated. above. Velocity calibration echnology (NIST), calibration, please contact
	A Hig	MARSH MCBIRNEY her Level of Flow Measurement	
(3	4539 Metropolita 801) 874-5599 ● (8 www	n Ct., Frederick, MD 2 00)-368-2723 • FAX (3 .marsh-mcbirney.com	1704-9452 301) 874-2172

Flowmeter Calibration Certificate.

Discharge Measurement: Bright Angel Spring, Rodman Reservoir/Ocklawaha River, Marion County, Florida; September 27, 2007



Prepared for: St. Johns River Water Management District

4049 Reid Street Palatka, Florida 32177

Prepared by:

# Karst Environmental Services, Inc.

5779 NE County Road 340 High Springs, Florida 32643 (386) 454-3556 (386) 454-3541 FAX kes@atlantic.net

# Discharge Measurement: Bright Angel Spring, Marion County, Florida; September 27, 2007

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# Results of Discharge Measurements of Bright Angel Spring, Marion County, Florida; September 27, 2007

## **INTRODUCTION**

The St. Johns River Water Management District (SJRWMD) contracted with Karst Environmental Services, Inc. (KES) to perform discharge measurements of the submerged springs that discharge into the Rodman Reservoir/Ocklawaha River, in Marion and Putnam Counties, Florida. This report documents the results of the measurement made at Bright Angel Spring on September 27, 2007. A summary of the results and collected data for that measurement are presented on Table 1.

## PURPOSE and SCOPE OF WORK

The purpose of this work was to obtain an initial discharge measurement of Bright Angel Spring, which is a source of groundwater discharge into the Rodman Reservoir/Ocklawaha River. A program of discharge measurements was to be made of the springs in the Rodman Reservoir/Ocklawaha River during September of 2007.

## SITE DESCRIPTION

Bright Angel Spring is located on the south side of the Rodman Reservoir and the Ocklawaha River channel, southeast of the public boat ramp at Kenwood Landing, at 416452 Easting/3265529 Northing (UTM Zone 17, NAD 1983 HARN, meters), or Lat. N29.516572°, Long. W81.862090° (WGS84).

The spring discharges primarily from a low, wide vent in bedrock at the bottom of a large basin. The vent was about 24 to 26 feet deep (during this measurement). The vent is about 10 feet wide, and has an opening with a maximum height of about 1.5 feet at its extreme right side (when viewed from downstream) and tapering to just a few inches high on the left. The vent was too small to allow for diver entry, and conditions around it during this measurement were very silty. See Figure 1.

Since the vent of this spring is located on the bottom of the river, its discharge cannot be measured by conventional discharge measurement methods. However, the spring vent opening provided a suitable location for a discharge measurement that lends itself to the application of an appropriately adapted instrument.

## PERSONNEL

Fieldwork for this discharge measurement was conducted by KES personnel Peter Butt and Tom Morris. Jeff Davis of the SJRWMD was also on site during the measurement, and provided logistics support. Data management and report preparation was performed by Peter Butt. Data processing using Surfer 8 contouring software was performed by W. Bruce Lafrenz, P.G., of Tetra Tech of Orlando, Florida.

## METHODS

#### Instrumentation

The instrument used for this discharge measurement was a Marsh-McBirney Model 2000 Flo-Mate electronic flowmeter (Serial Number 2002679) that has been adapted for fully submersible use. In order to operate and read the meter at depth, the unit has been placed within an underwater housing with a transparent lid. The sensor wire is routed through a sealing gland on the housing lid. There are two housing controls that allow for direct operation of the flow meter. One operates the on/off/reset buttons, and the other operates the time interval selector buttons that control the measurement period.

The flowmeter used was factory calibrated while in its underwater housing in the method normally used for this unit on April 20, 2007. A copy of the Calibration Certificate is included with this report.

A video record of the site was made on August 29, 2007.

#### Field Operations

Velocity measurements were taken at the 1.5 foot high end of the vent. The measurement site was 24-26 feet deep. The rest of the vent was blocked with plastic bubble wrap sheets to eliminate areas that could not be measured, and divert flow to the measurement cross-section. Cross-section dimensions were approximately 1.5 feet high by 2 feet wide.

Five telescoping aluminum poles with 0.1, 0.25, 0.5 and one-foot interval markings were positioned vertically and horizontally to provide a positioning grid for velocity measurements. As all sensor-support poles were positioned at right angles to the main flow path, no angle coefficient corrections for velocity readings were made. The flowmeter sensor was positioned on the poles with a low-profile metal spring clamp. Conduit dimensions around the grid were measured with a collapsible steel tape. See Figure 2.

Peter Butt positioned the sensor and recorded positional data, while Tom Morris took the velocity readings after taking reset cues from Butt. During all measurements, the sensor handler was able to move away from the measurement cross-section, and remove himself from the cross section of the flow. The meter operator was also positioned above and away from the cross-section. This minimized or eliminated the possibility of interference with flow while the measurements were taken. The flowmeter was operated in the "Fixed Point Averaging" mode. Fixed Point Averaging is an average of velocities over a fixed period of time. Averaging periods of 60 seconds were used. The flowmeter was reset between each station. Thirteen station readings were made.

#### Data Processing

Field measurements of the velocity measurement stations and vent boundaries were plotted on grid paper and assigned X- and Y-axis values. See Figure 2. Values for the Z-axis were the point velocities, and zero values were assigned to the cross-section boundary points. See Table 3. The X, Y and Z data was processed using the Surfer v.8 (by Golden Software, Inc.) contouring program. The gridding method used was point Kriging with linear drift, and anisotropy ratio of 1 at an angle of  $0^{\circ}$ , and a variogram slope of 1. The results of the contour processing are illustrated in Figures 3 and 4.

Discharge and measurement cross-section area are given on the Grid Volume Computations and Gridding Report feature of the software, included in this report on page 1 of Table 2. The total discharge is shown as the "**Net Volume (Cut-Fill)**". The Net Volume value is used because a Surfer 8 "blanking file" operation was used to define the measurement cross-section boundary and eliminate artifacts present in the contouring process that would create inaccuracies in the flow calculations. The software also calculated the total cross-sectional area of the measurement location within the passage, and is shown in square feet as the "**Positive Planar Area (Cut)**".

## **RESULTS AND DISCUSSION**

This measurement is the first one performed at Bright Angel Spring applying the method and data processing used at other spring sites by KES. Based on KES' experience at other springs, the estimate of discharge for this initial measurement should be considered to be a minimum value. The data from this measurement will also provide a guide for the planning and improvements for any future measurements of this type here.

The estimated discharge of Bright Angel Spring on September 27, 2007 was 0.445 CFS (cubic feet per second). This result is also expressed as 200 GPM (gallons per minute) or 0.288 MGD (million gallons per day), see Table 1. Thirteen (13) readings were made, see Figures 2 and 4. The point velocity readings ranged from 0.04 to 0.29 feet per second (fps), with an overall average station reading of 0.20 fps. The total cross-sectional area was calculated as 2.52 square feet. Individual point velocity measurement periods of 60 seconds were used. The measurements commenced at about 14:28 hours and were completed by 14:57.

UNDERWATE	R DISCHARGE N	IEASUREMENT		
Location:	on: BRIGHT ANGEL SPRING		Date:	September 27, 2007
Rodman Rese	rvoir/Ocklawaha F	River	Time Start:	14:28
Marion County, F		Florida	Time End:	14:57
Personnel:	Peter Butt, Tom M	orris		
Method: Grid within irregula		ar conduit		
Instrument:	MMB2000 FLO-M	ATE in U/W case, sen	sor on support pol	es
Analysis Method	I: Surfer 8 with krigir	ıg		
		-		
Bright Angel S	Spring Total Disc	harge:		
CFS	0.445			
 MGD	0.288			
GPM	200			
Total Cross-se	ctional Area:	2.52	square feet	
Avg. Station Point Velocity:		0.20	feet/second	
Cross-section Depth:		24-26	feet deep	
Msmt. Periods:		60 seconds		
Velocity Reading by Station:		(All velocity readings in feet per second.)		
Station #	Point Velocity			
1	0.15			
2	0.22			
3	0.29			
4	0.24			
5	0.04			
6	0.2			
7	0.28			
8	0.26			
9	0.28			
10	0.13			
11	0.2			
12	0.22			
13	0.09			



Figure 1. Underwater video still of Bright Angel Spring, Marion County, Florida. Measurement cross-section area is on the right side of the vent.



Figure 2. Discharge measurement cross-section; Bright Angel Spring, Marion County, Florida, September 27, 2007 measurement. Cross-section is viewed to the upstream of observer, and is located between the 24- to 26-foot depth levels. Velocity measurement stations are shown as numbered points. See Table 1 for station velocities. Boundary of cross section is shown as connected, lettered points. Support poles represented by dashed lines. X- and Y-axis scales are shown in feet.



Figure 3. Discharge measurement cross-section; Bright Angel Spring, Marion County, Florida, September 27, 2007 measurement. Flow contour velocities are shown in feet per second. Outer boundary of cross section represents the zero-value contour. X- and Y-axis scales are shown in feet.

# TABLE 2. BRIGHT ANGEL SPRING, SEPTEMBER 27, 2007.SURFER 8 GRID VOLUME COMPUTATIONS AND GRIDDING REPORT

## **UPPER SURFACE**

Grid File Name:	Y:\2. PROJECTS\KARST ENVIRONMENTAL\Rodman\bright
	angel\2007-09\BrightAngel_9-07.bln.grd
Grid Size:	81 rows x 121 columns
X Minimum:	0
X Maximum:	3
X Spacing:	0.025
Y Minimum:	0
Y Maximum:	2
Y Spacing:	0.025
Z Minimum:	-0.000265858310875
Z Maximum:	0.31638284826777

## LOWER SURFACE

Level Surface defined by Z = 0

## VOLUMES

Z Scale Factor:	1
Total Volumes by:	
Trapezoidal Rule:	0.44544245532653
Simpson's Rule:	0.44549858576893
Simpson's 3/8 Rule:	0.44543409662667

#### **CUT & FILL VOLUMES**

Positive Volume [Cut]:0.44544262731012Negative Volume [Fil]:1.7198358398693E-007Net Volume [Cut-Fill]:0.44544245532653<<<<<Total Discharge in CFS</th>(The Net Volume value is used due to the use of a blanking file operation in the calculations.Positive Vol. Cut - Negative Vol. Fill = Net Volume. Please refer to report text.)

#### AREAS

Planar Areas	
Positive Planar Area [Cut]:	2.5168358361802<<< <cross-section feet<="" in="" square="" th=""></cross-section>
Negative Planar Area [Fill]:	3.9163819753962E-005
Blanked Planar Area:	3.483125
Total Planar Area:	6

## **Surface Areas**

Positive Surface Area [Cut]:	2.970149017277
Negative Surface Area [Fill]:	4.0162044215428E-005

# **GRIDDING REPORT**

# **Data Source**

Source Data File Name:	Y:\2. PROJECTS\KARST ENVIRONMENTAL\Rodman\bright angel\2007-09\Bright Angel 9-07 SURFER XYZ T3BLF.xls
X Column:	A
Y Column:	В
Z Column:	C
Data Counts	
Active Data:	135
Original Data:	135
Excluded Data:	0
Deleted Duplicates:	0
Retained Duplicates:	0
Artificial Data:	0
Superseded Data:	0

# **Univariate Statistics**

	Х	Y	Z
Minimum:	0.5	0.2	0
25%-tile:	1	0.385	0
Median:	1.7	1	0
75%-tile:	2.4	1.65	0
Maximum:	2.5	1.8	0.29
Midrange:	1.5	1	0.145
Range:	2	1.6	0.29
Interquartile Range:	1.4	1.265	0
Median Abs. Deviation:	0.7	0.645	0
Mean:	1.6597148148148	1.0109259259259	0.019259259259259
Trim Mean (10%):	1.6728577235772	1.0113821138211	0.0083739837398374
Standard Deviation:	0.68737047949182	0.59111639048974	0.063358236386202
Variance:	0.47247817607682	0.34941858710562	0.0040142661179698
Coef. of Variation:			3.2897545815912
Coef. of Skewness:			3.2350898861509

# **Inter-Variable Correlation**

	Х	Y	Z	
<b>K</b> :	1.000	-0.000	0.005	
<i>ไ</i> :		1.000	0.051	
<u>Z:</u>			1.000	
### **Inter-Variable Covariance**

	Х	Y	Z
X: Y: Z:	0.47247817607682	-4.4106310013709E-005 0.34941858710562	0.00023512208504801 0.0019006858710562 0.0040142661179698

# **Planar Regression: Z** = **AX**+**BY**+**C**

## **Fitted Parameters**

	А	В	С
Parameter Value:	0.00049814365821325	0.0054396300382277	0.012933419816727
Standard Error:	0.0080123311148857	0.0093170143289772	0.017202174531924

# **Inter-Parameter Correlations**

	А	В	С	
A: B: C:	1.000	-0.000 1.000	-0.773 0.548 1.000	

# **ANOVA** Table

Source	df	Sum of Squares	Mean Square	F
Regression:	2	0.001411580591955	57	
	0.00070579029597	7784	0.17236	
Residual:	132	0.54051434533397	0.00409480564646	595
Total:	134	0.54192592592593		

Coefficient of Multiple Determination (R^2): 0.0026047482218974

## **Nearest Neighbor Statistics**

	Separation	Delta Z
Minimum:	0.05	0
25%-tile:	0.05	0
Median:	0.050249378105604	0
75%-tile:	0.054230987451825	0
Maximum:	0.5	0.28

Table 2. Bright Angel Spring, September 27, 2007.

Midrange:	0.275	0.14
Range:	0.45	0.28
Interquartile Range:	0.004230987451825	0
Median Abs. Deviation:	0.00024937810560467	0
Mean:	0.066286304330351	0.016222222222222
Trim Mean (10%):	0.055802762921756	0.0060975609756098
Standard Deviation:	0.057274727207928	0.055522656925788
Variance:	0.0032803943767426	0.0030827654320988
Coef. of Variation:	0.86405069322447 3.4	4226295365212
Coef. of Skewness:	5.3539694352169 3.5	5638003315434
Root Mean Square:	0.087602902454876	0.057843979167463
Mean Square:	0.0076742685185185	0.0033459259259259

# **Complete Spatial Randomness**

Lambda:	42.1875
Clark and Evans:	0.86108435209606
Skellam:	274.62142596877

# **Exclusion Filtering**

Exclusion Filter String: Not In Use

# **Duplicate Filtering**

Duplicate Points to Keep:	First
X Duplicate Tolerance:	2.3E-007
Y Duplicate Tolerance:	1.9E-007
No duplicate data were for	ınd.

### **Breakline Filtering**

Breakline Filtering: Not In Use

# **Gridding Rules**

Gridding Method:	Kriging
Kriging Type:	Point
Polynomial Drift Order:	1
Kriging std. deviation grid:	no

### **Semi-Variogram Model**

Component Type:	Linear
Anisotropy Angle:	0
Anisotropy Ratio:	1
Variogram Slope:	1

## **Search Parameters**

No Search (use all data): true

# **Output Grid**

Grid File Name:	Y:\2. PROJECTS\KARST ENVIRONMENTAL\Rodman\bright
	angel\2007-09\BrightAngel_9-07.grd
Grid Size:	81 rows x 121 columns
Total Nodes:	9801
Filled Nodes:	9801
Blanked Nodes:	0

# Grid Geometry

X Minimum:	0
X Maximum:	3
X Spacing:	0.025
Y Minimum:	0
Y Maximum:	2
Y Spacing:	0.025

### **Grid Statistics**

Z Minimum:	-0.23896026886856
Z 25%-tile:	-0.084321271676576
Z Median:	-0.029557250809516
Z 75%-tile:	0.15417492050885
Z Maximum:	0.31638284826777

Z Midrange:	0.038711289699605
Z Range:	0.55534311713633
Z Interquartile Range:	0.23849619218543
Z Median Abs. Deviation:	0.08643241801018

Z Mean:	0.023094483073074
Z Trim Mean (10%):	0.019771300553881
Z Standard Deviation:	0.14742174571651
Z Variance:	0.021733171110104
Z Coef. of Variation:	6.3834182930203
Z Coef. of Skewness:	0.53832497168732
Z Root Mean Square:	0.14921972476357
Z Mean Square:	0.022266526258516



Figure 4. Discharge measurement cross-section; Bright Angel Spring, Marion County, Florida, September 27, 2007 measurement. Relationship of flow contours (velocities shown in feet per second) and velocity measurement stations (numbered points) are shown. See Table 1 for station velocities. Boundary of cross section is shown as connected, lettered points. X- and Y-axis scales are shown in feet.

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Table 3. Br	right Angel Sp	ring XYZ Grid Da	ta September	27,	2007.	
Y	v	Z (Velocity)	Station #		X Plot	Y Plot
24	1		1		/8	20
2.4	1	0.13	2		40	20
1.5	1	0.22	2		30	20
1.5	1	0.29	3		20	20
0.75	1	0.24	5		15	20
0.75	1.5	0.04	5		13	20
2.4	1.5	0.2	0		40	30
1 5	1.55	0.20	0		40	22
1.5	1.05	0.20	0		30	22
2.4	1.05	0.20	9		20	33
2.4	0.5	0.13	10		40	10
2	0.5	0.2	11		40	10
1.5	0.5	0.22	12		30	10
1	0.5	0.09	13		20	10
0.5		~			10	20
0.5	1	0	A		10	20
0.75	0.5	0	В		15	10
1	0.2	0	C		20	4
1.5	0.25	0	D		30	5
2	0.4	0	E		40	8
2.5	0.25	0	F		50	5
2.5	1	0	G		50	20
2.5	1.7	0	Н		50	34
2	1.75	0	I		40	35
1.5	1.8	0	J		30	36
1	1.8	0	K		20	36
0.75	1.2	0	L		15	24
		0				
0.525	0.95	0	A1		10.5	19
0.55	0.9	0	A2		11	18
0.575	0.85	0	A3		11.5	17
0.6	0.8	0	A4		12	16
0.625	0.75	0	A5		12.5	15
0.65	0.7	0	A6		13	14
0.675	0.65	0	A7		13.5	13
0.7	0.6	0	A8		14	12
0.725	0.55	0	A9		14.5	11
		0				
0.7915	0.45	0	B1		15.83	9
0.833	0.4	0	B2		16.66	8
0.8745	0.35	0	B3		17.49	7
0.916	0.3	0	B4		18.32	6
0.9575	0.25	0	B5		19.15	5
		0				
1.05	0.205	0	C1		21	4.1
1.1	0.21	0	C2		22	4.2
1.15	0.215	0	C3		23	4.3

X	Y	Z (Velocity)	Station #	X Plot	Y Plot
1.2	0.22	0	C4	24	4.4
1.25	0.225	0	C5	25	4.5
1.3	0.23	0	C6	26	4.6
1.35	0.235	0	C7	27	4.7
1.4	0.24	0	C8	28	4.8
1.45	0.245	0	C9	29	4.9
1.55	0.265	0	D1	31	5.3
1.6	0.28	0	D2	32	5.6
1.65	0.295	0	D3	33	5.9
1.7	0.31	0	D4	34	6.2
1.75	0.325	0	D5	35	6.5
1.8	0.34	0	D6	36	6.8
1.85	0.355	0	D7	37	7.1
1.9	0.37	0	D8	38	7.4
1.95	0.385	0	D9	39	7.7
2.05	0.385	0	E1	41	7.7
2.1	0.37	0	E2	42	7.4
2.15	0.355	0	E3	43	7.1
2.2	0.34	0	E4	44	6.8
2.25	0.325	0	E5	45	6.5
2.3	0.31	0	E6	46	6.2
2.35	0.295	0	E7	47	5.9
2.4	0.28	0	E8	48	5.6
2.45	0.265	0	E9	49	5.3
2.5	0.3	0	F1	50	6
2.5	0.35	0	F2	50	7
2.5	0.4	0	F3	50	8
2.5	0.45	0	F4	50	9
2.5	0.5	0	F5	50	10
2.5	0.55	0	F6	50	11
2.5	0.6	0	F7	50	12
2.5	0.65	0	<b>F</b> 8	50	13
2.5	0.7	0	<b>F9</b>	50	14
2.5	0.75	0	F10	50	15
2.5	0.8	0	F11	50	16
2.5	0.85	0	F12	50	17
2.5	0.9	0	F13	50	18
2.5	0.95	0	F14	50	19
	4.05				
2.5	1.05	0	G1	50	21
2.5	1.1	0	G2	50	22
2.5	1.15	0	G3	50	23
2.5	1.2	0	G4	50	24
2.5	1.25	0	G5	50	25
2.5	1.3	0	G6	50	26

X	Y	Z (Velocity)	Station #	X Plot	Y Plot
2.5	1.35	0	G7	50	27
2.5	1.4	0	G8	50	28
2.5	1.45	0	G9	50	29
2.5	1.5	0	G10	50	30
2.5	1.55	0	G11	50	31
2.5	1.6	0	G12	50	32
2.5	1.65	0	G13	50	33
2.45	1.705	0	H1	49	34.1
2.4	1.71	0	H2	48	34.2
2.35	1.715	0	H3	47	34.3
2.3	1.72	0	H4	46	34.4
2.25	1.725	0	H5	45	34.5
2.2	1.73	0	H6	44	34.6
2.15	1.735	0	H7	43	34.7
2.1	1.74	0	H8	42	34.8
2.05	1.745	0	H9	41	34.9
1.95	1.755	0	l1	39	35.1
1.9	1.76	0	12	38	35.2
1.85	1.765	0	13	37	35.3
1.8	1.77	0	14	36	35.4
1.75	1.775	0	15	35	35.5
1.7	1.78	0	16	34	35.6
1.65	1.785	0	17	33	35.7
1.6	1.79	0	18	32	35.8
1.55	1.795	0	19	31	35.9
1.45	1.8	0	J1	29	36
1.4	1.8	0	J2	28	36
1.35	1.8	0	J3	27	36
1.3	1.8	0	J4	26	36
1.25	1.8	0	J5	25	36
1.2	1.8	0	J6	24	36
1.15	1.8	0	J7	23	36
1.1	1.8	0	J8	22	36
1.05	1.8	0	J9	21	36
0.979	1.75	0	K1	19.58	35
0.958	1.7	0	K2	19.16	34
0.937	1.65	0	K3	18.74	33
0.916	1.6	0	K4	18.32	32
0.895	1.55	0	K5	17.9	31
0.874	1.5	0	K6	17.48	30
0.853	1.45	0	K7	17.06	29
0.832	1.4	0	K8	16.64	28
0.811	1.35	0	K9	16.22	27
0.79	1.3	0	K10	15.8	26

Х	Y	Z (Velocity)	Station #	X Plot	Y Plot
0.769	1.25	0	K11	15.38	25
0.7	1.16	0	L1	14	23.2
0.65	1.12	0	L2	13	22.4
0.6	1.08	0	L3	12	21.6
0.55	1.04	0	L4	11	20.8

	CALIBRA	TION CERTIFIC	ATE
Model: 20	000	_Serial Number: 20	02679
Unit Gain Rat	io:	Time Cons	stant:
	,	Type of Reading	
Velocity:	1	Level:	
		Ī	N/A
	Static Velocity	Dynamic Velocity	Level
Standard:	Zero	2.00	NA
Measured:	0.00	2.00	NA
Factory (	Calibration		
Field Pro	file Calibration;	Authintion	
Site Coe	mcient or velocity iv	iumpner	
Calibration T	echnician:	/	Date: 4-20-07
Calibration	TRA		and for
QA Technicia	an:		_ Date:
This documo	nt cortifies that the (	described instrument h	as been calibrated
Verification is	indicated by the m	easured results show a	above. Velocity calibration
Gaithersburg	, MD. For product in	formation, service, or o	calibration, please contact
the Custome	r Service Departme		
		MARSH	
	A Hig	MCBIRNEY her Level of Flow Measurement	
	4539 Metropolita	n Ct., Frederick, MD 2	1704-9452 301) 874-2172
	WWW	.marsh-mcbirney.com	

Flowmeter Calibration Certificate.

Discharge Measurement: Fish Hook Spring #1, Rodman Reservoir/Ocklawaha River, Marion County, Florida; September 27, 2006

Prepared for:

**St. Johns River Water Management District** 

4049 Reid Street, Palatka, Florida 32177

Prepared by:

Karst Environmental Services, Inc.

5779 NE County Road 340, High Springs, Florida 32643 (386) 454-3556 (386) 454-3541 FAX kes@atlantic.net

# Discharge Measurement: Fish Hook Spring #1, Marion County, Florida; September 27, 2006

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- 1. Results of Discharge Measurements of Fish Hook Spring #1, Marion County, Florida; September 27, 2006.
- 2. Table 1. Discharge of Fish Hook Spring #1, Marion County, Florida on September 27, 2006. Data record and calculation of discharge measurement.
- 3. Figure 1. Underwater video still of Fish Hook Spring #1, Marion County, Florida.
- 4. Figure 2. Vent Discharge Capture Device (VDCD). Sensor is attached to and centered on the gray PVC tube at the top of the 0.5 foot diameter pipe.
- 5. Flowmeter Calibration Certificate.

# Results of Discharge Measurements of Fish Hook Spring #1, Marion County, Florida; September 27, 2006

## INTRODUCTION

The St. Johns River Water Management District (SJRWMD) contracted with Karst Environmental Services, Inc. (KES) to conduct discharge measurements of selected springs in the Rodman Reservoir/Ocklawaha River in Marion County, Florida. This report documents the results of the measurement made at Fish Hook Spring #1 on September 27, 2006.

### PURPOSE and SCOPE OF WORK

The purpose of this work is to obtain an initial discharge measurement of Fish Hook Spring #1, which is among the many sources of groundwater discharging into the Rodman Reservoir/Ocklawaha River. A program of discharge measurements was to be made of the springs in the Rodman Reservoir/Ocklawaha River during September of 2007.

#### PERSONNEL

Fieldwork for this discharge measurement was conducted by Peter Butt and Tom Morris, both of KES. Jeff Davis of the SJRWMD was also on site during the measurement, and provided logistics support. Data management and report preparation was performed by Peter Butt. W. Bruce Lafrenz, P.G., of Tetra Tech of Orlando, Florida provided oversight.

#### SITE DESCRIPTION

Fish Hook Spring #1 is comprised of a single small vent, less than two feet in diameter, and is about 8 feet deep. It is located at 412625 Easting/3264772 Northing (UTM Zone 17, NAD 1983 HARN, meters), or Lat. N29.509497°, Long. W81.901514° (WGS84). It lies just offshore of the south bank, in an area of heavy aquatic vegetation, and about 230 feet east of Fish Hook Spring #2. See Figure 1.

Since the vent of this spring is located on the bottom of the reservoir, its discharge cannot be measured by conventional discharge measurement methods. However, the spring vent opening provides a suitable location for a discharge measurement that lends itself to the application of an appropriately adapted instrument.

#### METHODS

#### Instrumentation

The instrument used for this discharge measurement was a Marsh-McBirney Model 2000 Flo-Mate electronic flowmeter (Serial Number 2002679) that has been adapted for fully submersible use. In order to operate and read the meter at depth, the unit has been placed within an underwater housing with a transparent lid. The sensor wire is routed through a sealing gland on the housing lid. There are two housing controls that allow for direct operation of the flow meter. One operates the on/off/reset buttons, and the other operates the time interval selector buttons that control the measurement period. The flowmeter used was factory calibrated while in its underwater housing in the method normally used for this unit on April 20, 2007. A copy of the Calibration Certificate is included with this report.

### Field Operations and Calculations

This spring consists of small, scattered vents discharging through a mixed bottom of either detritus, sediments, a thick algal layer, sand or pebbles. Direct measurements of the vent cross-sections at this site were not practical. To accomplish measurements of these vents, a device was designed and employed to capture and concentrate the vent discharge for effective measurement. This device is referred to herein as the Vent Discharge Capture Device (VDCD). See Figure 2.

The VDCD is constructed of an inverted heavy-duty plastic tub that has a plastic flange connecting it to a short length of plastic pipe. The tub dimensions are 2.23 feet inside diameter on its bottom, a height of 1.05 feet, and a top inside diameter of 1.8 feet. The top side of the tub has a 0.5 foot hole to which a flange is attached. A 0.49 foot inside diameter plastic discharge pipe is attached to the flange and extends upward for 2.05 feet. This minimum pipe length was chosen to minimize turbulence at the sensor placement location at its upper end.

A section of half-inch PVC pipe is inserted through holes on opposite sides of the discharge pipe near its top for positioning the flow sensor. The sensor has a spring clip that attaches it to the half-inch PVC pipe, and it is positioned facing downward in the center of the discharge pipe.

To install the VDCD over a spring vent for a measurement, the open end of the tub is centered over a vent and pushed down onto the bottom, often into the sediment or detritus. Belts of weights are placed around the flange area of the tub to securely hold it in place. Sediments were sometimes arranged around the bottom circumference of the tub to provide a more effective seal. The discharge pipe is kept in a vertical position. The sensor is positioned at a right angle to the main flow path within the discharge pipe, so no angle coefficient corrections for velocity readings are necessary.

Once in place, the installation is checked for leakage around its bottom circumference. The condition of nearby vents is monitored for changes in flow, or the formation of new vents. A few minutes are allowed to let debris clear and for conditions to stabilize. The sensor is monitored for debris accumulation and cleaned off as needed.

Once the VDCD and sensor are positioned, and positional data recorded, velocity readings are made. During all measurements, the sensor handler moved away from the discharge pipe, eliminating the possibility of interference while the measurements were taken. The flowmeter was operated in its Fixed Point Averaging mode. Fixed Point Averaging is an average of measured velocities over a fixed period of time. Averaging periods of 60 seconds were used. The flowmeter was reset between each reading. A record and the calculated results of these measurements are presented in Table 1.

To measure the discharge, a series of three readings are typically taken at each vent installation, and the average velocity determined. The discharge (Q) is calculated by multiplying the averaged velocity by the area of the pipe ( $Q = V \times pi \times r^2$ ). For purposes of this calculation, it is assumed that the measured velocity is representative of velocities over the entire cross-section.

This assumption is based on direct observations of the uniformity of flow exiting the pipe. In addition, the plastic pipe is smooth sided and relatively short in length.

### **RESULTS AND DISCUSSION**

This measurement is the first one performed at Fish Hook Spring #1 applying the method and data processing used at other spring sites by KES. Based on KES' experience at other springs, the estimate of discharge for this initial measurement should be considered to be a minimum value. The data from this measurement will also provide a guide for the planning and improvements for any future measurements of this type here.

The estimated discharge of Fish Hook Spring #1 on September 27, 2006 was 0.09 CFS (cubic feet per second). This result is also expressed as 40 GPM (gallons per minute) or 0.057 MGD (million gallons per day), see Table 1. Four readings were made. Individual point velocity readings ranged from 0.44 to 0.49 feet per second (fps), with an overall average station reading of 0.47 fps. Individual point velocity measurement periods of 60 seconds were used. The approximate depth for the measurements was 8 feet. The measurements commenced at about 16:00 hours and were completed by 16:10 hours.

UNDERWATE	R DISCHARGE I	MEASUREME	Т		
Location:	FISH HOOK SF	PRING #1		Date:	September 27, 2007
	Rodman Reserv	voir/Ocklawaha	River	Time Start:	16:00
	Marion County,	Florida		Time End:	16:10
Personnel:	Peter Butt, Tom N	Norris, Jeff Davis			
Method:	Vent Discharge C	apture Device	(0.49' Diameter)		
Instrument:	MMB2000 FLO-M	IATE in U/W cas	e, sensor in vertic	al pipe	
Calculation Meth	nod: Discharge = V	x <i>pi</i> x r <sup>2</sup>			
Measurement	Periods:	60 seconds			
 Fish Hook Spri	ng #1 Total Discha	arge:	Vent 1		
 CFS	0.09		0.088		
MGD	0.057		0.057		
GPM	40		40		
Vent Depth (feet d	eep):		8		
 	-				
 Velocity Read	lings:	(All velocity re	eadings in feet p	er second.)	
 Vent 1					
Reading #	Point Velocity				
1	0.44				
2	0.47				
3	0.47				
4	0.49				
Average:	0.47				
Discharge:	0.088				

Table 1. Discharge of Fish Hook Spring #1, Marion County, Florida on September 27, 2007 Data record and calculation of discharge measurement.



Figure 1. Underwater video still of Fish Hook Spring #1, Marion County, Florida.



Figure 2. Vent Discharge Capture Device (VDCD). Sensor is attached to and centered on the gray PVC tube at the top of the 0.5 foot diameter pipe.

CALI	BRATION CERTIFIC	CATE
Model: 2000	Serial Number: c	02679
Unit Gain Ratio:	Time Cons	stant:
	Type of Reading	
Valasitur	Lovel:	
FPS	Levei.	
		N/A
Static Velo	Dynamic Velocity	Level
Standard: <u>Zero</u>	2.00	NA
	7.00	NA
Measured:		<u>_/</u>
M Factory Calibration		
Pactory Calibration		
Field Profile Calibratio	on;	
Site Coefficient or Ve	locity Multiplier:	
Calibration Technician:		Date: 4-20-07
	A	and by
QA Technician:	× .	Date:
This document certifies th	at the described instrument h	as been calibrated.
Verification is indicated by is traceable to the Nationa	y the measured results show a al Institute of Standards and T	above. Velocity calibration echnology (NIST),
Gaithersburg, MD. For pro	oduct information, service, or partment.	calibration, please contact
	$\sim$	
	MARSH	
	A Higher Level of Flow Measurement	1704 0452
4539 Met (301) 874-55	99 • (800)-368-2723 • FAX (	301) 874-2172
	www.marsh-mcbirney.com	

Discharge Measurement: Catfish Convention Hall Spring, Silver Springs, Group, Marion County, Florida; September 11, 2007



Prepared for: **St. Johns River Water Management District** 4049 Reid Street, Palatka, Florida 32177

Prepared by: **Karst Environmental Services, Inc.** 5779 NE County Road 340, High Springs, Florida 32643 (386) 454-3556 (386) 454-3541 FAX kes@atlantic.net

# Discharge Measurement: Catfish Convention Hall Spring, Silver Springs Group, Marion County, Florida; September 11, 2007

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- 1. Results of Discharge Measurements of Catfish Convention Hall Spring, Marion County, Florida; September 11, 2007.
- 2. Table 1. Discharge of Catfish Convention Hall Spring, Marion County, Florida on September 11, 20076. Data record and calculation of discharge measurement.
- 3. Figure 1. Map of Catfish Convention Hall Spring, Silver Springs Group, Marion County, Florida.
- 4. Figure 2. Underwater photograph of Catfish Convention Hall Spring, Silver Springs Group, Marion County, Florida. Vents that comprise this spring lie in front of the diver.
- 5. Figure 3. Underwater photograph of Catfish Convention Hall Spring vent, Silver Springs Group, Marion County, Florida. This area contains the main vent cluster.
- 6. Figure 4. Vent Discharge Capture Device (VDCD). Sensor is attached to and centered on the gray PVC tube at the top of the 0.5 foot diameter pipe.
- 7. Flowmeter Calibration Certificate.

# Results of Discharge Measurements of Catfish Convention Hall Spring, Marion County, Florida; September 11, 2007

## INTRODUCTION

The St. Johns River Water Management District (SJRWMD) contracted with Karst Environmental Services, Inc. (KES) to conduct a series of discharge measurements at the Silver Springs Group in Marion County, Florida. This report documents the results of the measurement made at Catfish Convention Hall Spring on September 11, 2007.

### PURPOSE and SCOPE OF WORK

The purpose of this work is to obtain an initial discharge measurement of Catfish Convention Hall Spring, which is among the many sources of groundwater discharging into the Silver River. A program of discharge measurements was to be made of the springs in the Silver Springs Group during September of 2007.

### PERSONNEL

Fieldwork for this discharge measurement was conducted by Peter Butt, Tom Morris and Mark Long, both of KES. Data management and report preparation was performed by Peter Butt. W. Bruce Lafrenz, P.G., of Tetra Tech of Orlando, Florida provided oversight.

#### SITE DESCRIPTION

Catfish Convention Hall Spring is comprised of two clusters of small vents, and a few additional scattered vents, about 20 feet deep, and located directly downstream from Shipwreck Spring and the bow of the namesake sunken boat. They lie in the eastern end of the basin that is an extension of the Shipwreck Spring basin. See Figure 1. The main vent cluster contains about five small vents within an area of about six feet in diameter, all discharging through sediments. Six vent locations were identified for measurement. See Figures 2 and 3.

Since the vents of this spring are located on the bottom of the river, its discharge cannot be measured by conventional discharge measurement methods. However, at the spring opening there is a suitable location for a discharge measurement that lends itself to the application of an appropriately adapted instrument.

#### METHODS

#### Instrumentation

The instrument used for this discharge measurement was a Marsh-McBirney Model 2000 Flo-Mate electronic flowmeter (Serial Number 2002679) that has been adapted for fully submersible use. In order to operate and read the meter at depth, the unit has been placed within an underwater housing with a transparent lid. The sensor wire is routed through a sealing gland on the housing lid. There are two housing controls that allow for direct operation of the flow meter. One operates the on/off/reset buttons, and the other operates the time interval selector buttons that control the measurement period. The flowmeter used was factory calibrated while in its underwater housing in the method normally used for this unit on April 20, 2007. A copy of the Calibration Certificate is included with this report.

### Field Operations

This spring consists of small, scattered vents discharging through a mixed bottom of either detritus, sediments, a thick algal layer, sand or pebbles. See Figure 3. Direct measurements of the vent cross-sections at this site were not practical. To accomplish measurements of these vents, a device was designed and employed to capture and concentrate the vent discharge for effective measurement. This device is referred to herein as the Vent Discharge Capture Device (VDCD). See Figure 4.

The VDCD is constructed of an inverted heavy-duty plastic tub that has a plastic flange connecting it to a short length of plastic pipe. The tub dimensions are 2.23 feet inside diameter on its bottom, a height of 1.05 feet, and a top inside diameter of 1.8 feet. The top side of the tub has a 0.5 foot hole to which a flange is attached. A 0.49 foot inside diameter plastic discharge pipe is attached to the flange and extends upward for 2.05 feet. This minimum pipe length was chosen to minimize turbulence at the sensor placement location at its upper end.

A section of half-inch PVC pipe is inserted through holes on opposite sides of the discharge pipe near its top for positioning the flow sensor. The sensor has a spring clip that attaches it to the half-inch PVC pipe, and it is positioned facing downward in the center of the discharge pipe.

To install the VDCD over a spring vent for a measurement, the open end of the tub is centered over a vent and pushed down onto the bottom, often into the sediment or detritus. Belts of weights are placed around the flange area of the tub to securely hold it in place. Sediments were sometimes arranged around the bottom circumference of the tub to provide a more effective seal. The discharge pipe is kept in a vertical position. The sensor is positioned at a right angle to the main flow path within the discharge pipe, so no angle coefficient corrections for velocity readings are necessary.

Once in place, the installation is checked for leakage around its bottom circumference. The condition of nearby vents is monitored for changes in flow, or the formation of new vents. A few minutes are allowed to let debris clear and for conditions to stabilize. The sensor is monitored for debris accumulation and cleaned off as needed.

Once the VDCD and sensor are positioned, and positional data recorded, velocity readings are made. During all measurements, the sensor handler moved away from the discharge pipe, eliminating the possibility of interference while the measurements were taken. The flowmeter was operated in its Fixed Point Averaging mode. Fixed Point Averaging is an average of measured velocities over a fixed period of time. Averaging periods of 60 seconds were used. The flowmeter was reset between each reading. A record and the calculated results of these measurements are presented in Table 1.

### Data Processing

To measure the discharge, a series of three readings are typically taken at each vent installation, and the average velocity determined. The discharge (Q) is calculated by multiplying the averaged velocity by the area of the pipe ( $Q = V \times pi \times r^2$ ). For purposes of this calculation, it is

assumed that the measured velocity is representative of velocities over the entire cross-section. This assumption is based on direct observations of the uniformity of flow exiting the pipe. In addition, the plastic pipe is smooth sided and relatively short in length.

It was often impractical or impossible to capture and quantify all of a spring's discharge at its various vents using this device. The reasons include; leakage, large size of vents, backpressure effects at adjacent vents, vents formed on long, narrow fissures and the presence of small vents too numerous and scattered to effectively measure. To better estimate the actual discharge, a multiplier was applied to the measurement results of some individual vents and lines of vents in order to account for water that would be otherwise missed at and beyond the measurement locations. While applying this multiplier to a measured discharge adds some element of subjectivity to that measurement, it is felt that this method provides a more accurate description in a difficult measurement situation. When used, these multipliers and resulting values are included in Table 1, and identified therein as "Estimated Discharge", and are presented along with the original "Measured Discharge" value.

### **RESULTS AND DISCUSSION**

This measurement is the second one of this type performed at Catfish Convention Hall Spring by KES. Based on KES' experience at other springs, the estimate of discharge for this initial measurement should be considered to be a minimum value. The data from this measurement will also provide a guide for the planning and improvements for any future measurements of this type here.

The estimated discharge of Catfish Convention Hall Spring on September 11, 2007 was 0.546 CFS (cubic feet per second). This result is also expressed as 245 GPM (gallons per minute) or 0.353 MGD (million gallons per day), see Table 1. Three readings were made at each of six vents, for a total of eighteen (18) readings. Individual point velocity readings ranged from 0.13 to 0.87 feet per second (fps), with an overall average station reading of 0.48 fps. Individual point velocity measurement periods of 60 seconds were used. The approximate depth for the measurements was 19 to 20 feet. The measurements commenced at about 10:27 hours and were completed by 11:06 hours.

UNDERWATER	DISCHARGE ME	ASUREMENT						
Location:	CATFISH CON	VENTION HALL SI	PRING	Date:	September 11	, 2007		
	Silver Springs G	Group,		Time Start:	10:27			
	Marion County,	Florida		Time End:	11:06			
Personnel:	Peter Butt, Tom N	Iorris, Mark Long						
Method:	Vent Discharge C	apture Device		(0.49' Diameter)				
Instrument:	MMB2000 FLO-N	IATE in U/W case, se	nsor in vertical pipe					
Calculation Method	d: Discharge = V x p	i x r <sup>2</sup>						
Measurement Pe	eriods:	60 seconds						
Catfish Conventio	I Hall Spring Tota	I Discharge:	Vent 1	Vent 2	Vent 3	Vent 4	Vent 5	Vent 6
CFS	0.546		0.069	0.093	0.028	0.133	0.163	0.060
MGD	0.353		0.045	0.060	0.018	0.086	0.105	0.039
GPM	245	All Vents:	31	42	12	60	73	27
Avg. Point Velocity (f	t/sec):	0.48	0.37	0.49	0.15	0.71	0.86	0.32
Vent Depth (feet deep	p):	19-20	19	19	19	19	19	19
Velocity Readin	gs:	(All velocity readir	l ngs in feet per sec	cond.)				
Ver	nt 1	Ven	t 2	Ve	nt 3	Ve	ent 4	
Tagge	ed vent							
Reading #	Point Velocity	Reading #	Point Velocity	Reading #	Point Velocity	Reading #	Point Velocity	
1	0.37	1	0.49	1	0.13	1	0.7	
2	0.36	2	0.5	2	0.16	2	0.71	
3	0.37	3	0.49	3	0.15	3	0.71	
Average:	0.37	Average:	0.49	Average:	0.15	Average:	0.71	
Discharge:	0.069	Discharge:	0.093	Discharge:	0.028	Discharge:	0.133	
Ver	nt 5	Ven	t 6					
Reading #	Point Velocity	Reading #	Point Velocity					
1	0.86	1	0.31					
2	0.86	2	0.32					
3	0.87	3	0.32					
Average:	0.86	Average:	0.32					
Discharge:	0.400	Disabarga	0.060					

Table 1. Discharge of Catfish Convention Hall Spring, Silver Springs Group, Marion County, Florida on September 11, 2007. Data record and calculation of discharge measurement.



Figure 1. Map of Catfish Convention Hall Spring, Silver Springs Group, Marion County, Florida.



Figure 2. Underwater photograph of Catfish Convention Hall Spring, Silver Springs Group, Marion County, Florida. Vents that comprise this spring lie in front of the diver.



Figure 3. Underwater photograph of Catfish Convention Hall Spring vent, Silver Springs Group, Marion County, Florida. This area contains the main vent cluster.



Figure 4. Vent Discharge Capture Device (VDCD). Sensor is attached to and centered on the gray PVC tube at the top of the 0.5 foot diameter pipe.

CA	LIBRATION	CERTIFIC	ATE	
Model: 2000	Serial I	Number: 206	2679	
Unit Gain Ratio:		Time Consta	ant:	
	Type of R	Reading		
Velocity:		Level:	IN	
	;		СМ	
U	—	Le	f N/A	
Static	/elocity Dyna	mic Velocity	Level	
Standard: Ze	ro	2.00	NA	
Monsurad:	20 2	.00	NA	
Measured	<u> </u>			
A Factory Calibration	n			
_				
Site Coefficient or	ration; Velocity Multiplier:			
	1			
Calibration Technician	- And		Date: <u>4-20-</u>	07
QA Technician:	BA.		Date: 2014	67
	0.00.1.0		/	
Verification is indicate	d by the measured	results show ab	ove. Velocity calibrated.	ation
Gaithersburg, MD. For the Customer Service	product informatio	n, service, or ca	libration, please cor	ntact
		-		
	MAI	RSH		
4500	A Higher Level of F	low Measurement	704 0452	
4539 I (301) 874	-5599 • (800)-368-	2723 • FAX (30	1) 874-2172	
	www.indisii=ii	iobinity.com		

Discharge Measurement: Lost River Spring, Silver Springs Group, Marion County, Florida; September 11, 2007



Prepared for: **St. Johns River Water Management District** 4049 Reid Street, Palatka, Florida 32177

Prepared by: **Karst Environmental Services, Inc.** 5779 NE County Road 340, High Springs, Florida 32643

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# Discharge Measurement: Lost River Spring, Silver Springs Group, Marion County, Florida; September 11, 2007

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- 6. Flowmeter Calibration Certificate.

# Results of Discharge Measurements of Lost River Spring, Marion County, Florida; September 11, 2007

## INTRODUCTION

The St. Johns River Water Management District (SJRWMD) contracted with Karst Environmental Services, Inc. (KES) to conduct a series of discharge measurements at the Silver Springs Group in Marion County, Florida. This report documents the results of the measurement made at Lost River Spring on September 11, 2007.

### PURPOSE and SCOPE OF WORK

The purpose of this work is to obtain an initial discharge measurement of Lost River Spring, which is among the many sources of groundwater discharging into the Silver River. A program of discharge measurements was to be made of the springs in the Silver Springs Group during September of 2007.

#### PERSONNEL

Fieldwork for this discharge measurement was conducted by Peter Butt, Tom Morris and Mark Long, both of KES. Data management and report preparation was performed by Peter Butt. W. Bruce Lafrenz, P.G., of Tetra Tech of Orlando, Florida provided oversight.

#### SITE DESCRIPTION

Lost River Spring is located about 70 feet east of the main linear vent of the Garden of Eden Springs Group and east of the Jungle Cruise boat dock Log Spring lies about 40 feet further upstream of Lost River Spring. The run for Lost River and Log Spring is log choked and slough-like. See Figure 1.

Lost River Spring is comprised of a vent that is about 10 feet deep and roughly two feet in diameter. It discharges gently through bottom sediments and a matrix of logs, branches and filamentous algae. See Figure 2.

Since the vents of this spring are located on the bottom of the river, its discharge cannot be measured by conventional discharge measurement methods. However, at the spring opening there is a suitable location for a discharge measurement that lends itself to the application of an appropriately adapted instrument.

#### **METHODS**

#### Instrumentation

The instrument used for this discharge measurement was a Marsh-McBirney Model 2000 Flo-Mate electronic flowmeter (Serial Number 2002679) that has been adapted for fully submersible use. In order to operate and read the meter at depth, the unit has been placed within an underwater housing with a transparent lid. The sensor wire is routed through a sealing gland on the housing lid. There are two housing controls that allow for direct operation of the flow meter. One operates the on/off/reset buttons, and the other operates the time interval selector buttons that control the measurement period.

The flowmeter used was factory calibrated while in its underwater housing in the method normally used for this unit on April 20, 2007. A copy of the Calibration Certificate is included with this report.

### Field Operations

This spring consists of a vent discharging through a mixed bottom of logs, detritus, sediments and a thick algal layer. See Figure 2. Direct measurements of the vent cross-sections at this site were not practical. To accomplish measurements of these vents, a device was designed and employed to capture and concentrate the vent discharge for effective measurement. This device is referred to herein as the Vent Discharge Capture Device (VDCD). See Figure 3.

The VDCD is constructed of an inverted heavy-duty plastic tub that has a plastic flange connecting it to a short length of plastic pipe. The tub dimensions are 2.23 feet inside diameter on its bottom, a height of 1.05 feet, and a top inside diameter of 1.8 feet. The top side of the tub has a 0.5 foot hole to which a flange is attached. A 0.49 foot inside diameter plastic discharge pipe is attached to the flange and extends upward for 2.05 feet. This minimum pipe length was chosen to minimize turbulence at the sensor placement location at its upper end.

A section of half-inch PVC pipe is inserted through holes on opposite sides of the discharge pipe near its top for positioning the flow sensor. The sensor has a spring clip that attaches it to the half-inch PVC pipe, and it is positioned facing downward in the center of the discharge pipe.

To install the VDCD over a spring vent for a measurement, the open end of the tub is centered over a vent and pushed down onto the bottom, often into the sediment or detritus. Belts of weights are placed around the flange area of the tub to securely hold it in place. Sediments were sometimes arranged around the bottom circumference of the tub to provide a more effective seal. The discharge pipe is kept in a vertical position. The sensor is positioned at a right angle to the main flow path within the discharge pipe, so no angle coefficient corrections for velocity readings are necessary.

Once in place, the installation is checked for leakage around its bottom circumference. The condition of nearby vents is monitored for changes in flow, or the formation of new vents. A few minutes are allowed to let debris clear and for conditions to stabilize. The sensor is monitored for debris accumulation and cleaned off as needed.

Once the VDCD and sensor are positioned, and positional data recorded, velocity readings are made. During all measurements, the sensor handler moved away from the discharge pipe, eliminating the possibility of interference while the measurements were taken. The flowmeter was operated in its Fixed Point Averaging mode. Fixed Point Averaging is an average of measured velocities over a fixed period of time. Averaging periods of 60 seconds were used. The flowmeter was reset between each reading. A record and the calculated results of these measurements are presented in Table 1.

### Data Processing

To measure the discharge, a series of three readings are typically taken at each vent installation, and the average velocity determined. The discharge (Q) is calculated by multiplying the averaged velocity by the area of the pipe ( $Q = V \times pi \times r^2$ ). For purposes of this calculation, it is assumed that the measured velocity is representative of velocities over the entire cross-section. This assumption is based on direct observations of the uniformity of flow exiting the pipe. In addition, the plastic pipe is smooth sided and relatively short in length.

It was often impractical or impossible to capture and quantify all of a spring's discharge at its various vents using this device. The reasons include; leakage, large size of vents, backpressure effects at adjacent vents, vents formed on long, narrow fissures and the presence of small vents too numerous and scattered to effectively measure. To better estimate the actual discharge, a multiplier was applied to the measurement results of some individual vents and lines of vents in order to account for water that would be otherwise missed at and beyond the measurement locations. While applying this multiplier to a measured discharge adds some element of subjectivity to that measurement, it is felt that this method provides a more accurate description in a difficult measurement situation. When used, these multipliers and resulting values are included in Table 1, and identified therein as "Estimated Discharge", and are presented along with the original "Measured Discharge" value.

## **RESULTS AND DISCUSSION**

This measurement is the first one performed at Lost River Spring applying the method and data processing used at other spring sites by KES. Based on KES' experience at other springs, the estimate of discharge for this initial measurement should be considered to be a minimum value. The data from this measurement will also provide a guide for the planning and improvements for any future measurements of this type here.

The estimated discharge of Lost River Spring on September 11, 2007 was 0.253 CFS (cubic feet per second). This result is also expressed as 113 GPM (gallons per minute) or 0.163 MGD (million gallons per day), see Table 1. Three readings were made at one vent. Individual point velocity readings ranged from 0.88 to 0.91 feet per second (fps), with an overall average station reading of 0.89 fps. Individual point velocity measurement periods of 60 seconds were used. The approximate depth for the measurements was 10 feet. The measurements commenced at about 16:48 hours and were completed by 16:52 hours.

UNDERWATER	DISCHARGE ME	ASUREMENT		
Location:	LOST RIVER S	PRING	Date:	September 11, 2007
	Silver Springs Group,		Time Start:	16:48
	Marion County,	Marion County, Florida		16:52
Personnel:	Peter Butt, Tom Morris, Mark Long			
Method:	Vent Discharge Capture Device		(0.49' Diameter)	
Instrument:	MMB2000 FLO-MATE in U/W case, se		ensor in vertical pipe	•
Calculation Method	d: Discharge = V x µ	$pi \ge r^2$		
Measurement Peri	Measurement Periods:			
Lost River Sprin	na ESTIMATED D	) Discharge:		
CFS	0.253			
MGD	0.163			
GPM	113			
(Multiplier:)	(1.5)			
Lost River Sprin	ng Measured Dis	charge:		
CFS	0.169			
MGD	0.109			
GPM	76			
Avg. Point Velocity (f	Avg. Point Velocity (ft/sec):			
Vent Depth (feet dee	Vent Depth (feet deep):			
Velocity Readin	Velocity Poadings:		(All velocity readings in feet per second	
Velocity Readin	lgs.			
Reading #	Point Velocity			
1	0.91			
2	0.89			
3	0.88			
Average:	0.89			
Discharge:	0.169			
Multiplier:	1.5			
Est.	0.253			
Discharge:				

Table 1. Discharge of Lost River Spring, Marion County, Florida on September 11, 2007. Data record and calculation of discharge measurement.



Figure 1. Map showing location of Lost River Spring, Silver Springs Group, Marion County, Florida.



Figure 2. Underwater photograph of Lost River Spring, Silver Springs Group, Marion County, Florida.



Figure 3. Vent Discharge Capture Device (VDCD). Sensor is attached to and centered on the gray PVC tube at the top of the 0.5 foot diameter pipe.

(	ALIBRAT	ION CERTIFIC	ATE
Model: 2000 Unit Gain Ratio:	<u> </u>	Serial Number: <u>20</u> Time Cons	<u> </u>
	Ty	pe of Reading	
Velocity:	PS	Level:	_ ім
	MS	Ĺ	L CM N/A
Stat	ic Velocity	Dynamic Velocity	Level
Standard: _	Zero	2.00	NA
Measured:	0.00	2.00	NA
Pactory Calibra	tion		•
Field Profile Ca	libration;	tislier	
Site Coefficient	or velocity mu	upner	
Calibration Technic	ian:		Date:7
OA Tashnisiani	RA		Date: 20151-07
This document cert Verification is indica is traceable to the N Gaithersburg, MD. the Customer Servi	ifies that the det ated by the mea National Institute For product info ce Department.	scribed instrument ha sured results show a of Standards and To rmation, service, or c	as been calibrated. bove. Velocity calibration echnology (NIST), calibration, please contact
	N	<b>LARSH</b> ICBIRNEY	
453	A Higher	Level of Flow Measurement Ct. Frederick MD 21	1704-9452
(301) 8	74-5599 • (800 www.m	)-368-2723 • FAX (3 arsh-mcbirney.com	01) 874-2172
Discharge Measurement: Mammoth Spring, Silver Springs Group, Marion County, Florida; September 10, 2007



Prepared for: St. Johns River Water Management District

4049 Reid Street, Palatka, Florida 32177

Prepared by: Karst Environmental Services, Inc.

5779 NE County Road 340, High Springs, Florida 32643 (386) 454-3556 (386) 454-3541 FAX kes@atlantic.net

# Discharge Measurement: Mammoth Spring, Silver Springs Group, Marion County, Florida; September 10, 2007

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# Results of Discharge Measurements of Mammoth Spring, Marion County, Florida; September 10, 2007

### **INTRODUCTION**

The St. Johns River Water Management District (SJRWMD) contracted with Karst Environmental Services, Inc. (KES) to conduct a discharge measurement at Mammoth Spring of the Silver Springs Group in Marion County, Florida. This report documents the results of the measurement made at the site on September 10, 2007. A summary of the results and collected data for that measurement are presented in Table 1.

#### PURPOSE and SCOPE OF WORK

The purpose of this work was to obtain accurate discharge measurements of the Mammoth Spring, the headspring and major source of groundwater discharge into the Silver River. A discharge measurement was to be made at the vent of Mammoth Spring during September, 2007.

#### SITE DESCRIPTION

Mammoth Spring is the largest spring of the Silver Springs Group, and is the headspring of the Silver River. The spring lies within a spring pool surrounded by the Silver Springs theme park. Mammoth Spring's vent is a wide, oval-shaped opening about 69 feet across, with floor to ceiling heights that vary from under 2 to over 6 feet. The depth of this vent ranges between 25 and 34 feet deep. The rock that comprises the ceiling of this vent is solid and self-supported, with the floor beneath composed of a layer of boulders and rubble. See Figure 1.

A large cavern with a complex network of cave passages lies inside of this vent. These cave passages supply waters of varying characteristics to the cavern, where some mixing occurs before these waters exit the vent. The inside of the cavern is a complex structure of breakdown boulders, bedding planes, and small passageways. It was determined during prior investigations that discharge measurements of individual water sources within the cavern would be problematic, if not impossible. The outer edge of this spring vent provided the best location for an underwater discharge measurement with an appropriately adapted instrument.

#### PERSONNEL

Fieldwork for this discharge measurement was conducted by KES personnel Peter Butt, Tom Morris, Mark Long and Wayne Kinard. Data management and report preparation was performed by Peter Butt. Data processing using Surfer 8 contouring software was performed by W. Bruce Lafrenz, P.G., of Tetra Tech of Orlando, Florida.

#### **METHODS**

#### **Instrumentation**

The instrument used for this discharge measurement was a Marsh-McBirney Model 2000 Flo-Mate electronic flowmeter (Serial Number 2002679) that has been adapted for fully submersible use. In order to operate and read the meter at depth, the unit has been placed within an underwater housing with a transparent lid. The sensor wire is routed through a sealing gland on the housing lid. There are two housing controls that allow for direct operation of the flow meter. One operates the on/off/reset buttons, and the other operates the time interval selector buttons that control the measurement period.

The flowmeter used was factory calibrated while in its underwater housing in the method normally used for this unit on April 20, 2007. A copy of the Calibration Certificate is included with this report.

#### Field Operations

Velocity measurements were taken just inside the ceiling edge of the vent. At the measurement site, the floor of the vent was 34 feet deep, and the ceiling was 26 feet deep.

A positioning grid of telescoping aluminum poles with 0.1, 0.25, 0.5 and one-foot interval markings that provided support for the sensor was set up by Pete Butt. Butt also recorded measurements of the grid and surrounding walls. Seventeen poles were positioned vertically to provide the primary positioning grid for velocity measurements. Eight horizontal poles were used as a spacing reference, and fastened to the vertical poles for support. Conduit dimensions around the grid were measured with a collapsible steel tape. As all sensor-support poles were positioned at roughly right angles to the main flow path, no angle coefficient corrections for velocity readings were made. The flowmeter sensor was attached to the poles with a low-profile metal spring clamp. Most measurement stations were set using one-foot intervals on the vertical poles. Velocity stations and boundary points are identified with alpha-numeric labels, based on the letter assigned to identify each vertical pole. See Figure 2.

Tom Morris positioned the sensor and recorded positional data. Mark Long took the velocity readings after taking reset cues from Morris, and also recorded positional data. During all measurements, the sensor handler was able to move away from the measurement cross-section, and remove himself from the cross section of the flow. The meter operator was also positioned downstream and away from the cross-section. This minimized or eliminated the possibility of interference with flow while the measurements were taken. The flowmeter was operated in the "Fixed Point Averaging" mode. Fixed Point Averaging is an average of velocities over a fixed period of time. Averaging periods of 60 seconds were used. The flowmeter was reset between each station. One-hundred and thirty-two (132) station readings were made.

#### Data Processing

Field measurements of the velocity measurement stations and vent boundaries were plotted on grid paper and assigned X- and Y-axis values. See Figure 1. Values for the Z-axis were the point velocities, and zero values were assigned to the cross-section boundary points. See Table 3. The X, Y and Z data was processed using the Surfer v.8 (by Golden Software, Inc.) contouring program. The gridding method used was point Kriging with linear drift, an anisotropy ratio of 3 at an angle of  $0^{\circ}$ , and a variogram slope of 1.0. The anisotropy ratio used was selected due to the extremely elongated horizontal aspect of the measurement cross-section. The results of the contour processing are illustrated in Figures 3 and 4.

During this measurement, two negative velocities were measured. These negative velocity stations represent slight back eddies near walls. In order to incorporate these negative values, calculations were made using a Surfer 8 "blanking file" operation to define the measurement cross-section boundary. The blanking file operation also assists in the elimination of artifacts present in the contouring process that would create inaccuracies in the flow calculations.

The total discharge is shown on Table 2 as the **Net Volume (Cut-Fill)**, and has been calculated as the Positive Volume (Cut) less that portion of the Negative Volume (Fill) lying within the measurement cross-section boundary walls that define the plane of measurement.

The software also calculates the total cross-sectional area of the measurement location within the passage, and is presented on page 1 of Table 2 as the **Operational Planar Area**. The Operational Planar Area is the sum of the Positive (Cut) and that portion of the Negative (Fill) Planar areas lying within the measurement cross-section boundary walls that define the plane of measurement.

## **RESULTS AND DISCUSSION**

This measurement is the third one performed at Mammoth Spring applying the method and data processing used at other spring sites by KES. This measurement also represents the largest cross-section and amount of discharge measured to date by KES. Based on KES' experience at other springs, the estimate of discharge for this measurement should be considered to be a minimum value. Based on results of the prior measurement performed here, additional velocity station readings close to the boundary walls of the cross-section were made to provide the additional data needed for Surfer to more accurately account for the higher flows present near the boundary edge and adjust the contours more appropriately. Due to the extremely elongated cross-section, a high anisotropy ratio setting was used to minimize a "bull's eye" or "curtain" effect that occurs in the contouring and has the unwanted effect of lowering the actual discharge value.

The estimated discharge of Mammoth Spring on September 10, 2007 was 207.78 CFS (cubic feet per second). This result is also expressed as 93258 GPM (gallons per minute) or 134.291 MGD (million gallons per day), see Table 1. One-hundred and thirty-two (132) readings were made, see Figures 2, 3 and 4. The point velocity readings ranged from -0.06 to 0.96 feet per second (fps), with an overall average station reading of 0.61 fps. The total cross-sectional area was calculated as 321.36 square feet. Individual point velocity measurement periods of 60 seconds were used. The measurements commenced at about 12:50 hours and were completed by 16:42 hours.

UNDERWATER DISCHARGE MEASUREMENT					
Location:	Location: MAMMOTH SPRING (Silver Springs Group) Marion Cou			Marion County,	Florida
Personnel:	Peter Butt, Tom Morris, Mark Long, Wayne Kinard			-	1
Method:	Grid within irregular conduit/cross-section				
Instrument:	trument: MMB2000 FLO-MATE in U/W case, sensor on support poles				
Analysis Method	: Surfer 8 with krig	ing			
Mommoth Sn	ing Total Disch		Deter	Sontombor 10	2007
		arge:	Time Stort	September 10,	2007
	207.78			12.50	
MGD	134.291		Time End:	16:42	
GPM	93258				
Total Cross-se	ctional Area:	321.36	square feet		
Avg. Station Po	oint Velocity:	0.61	feet/second		
Cross-section	Depth:	26-34	feet deep		
Msmt. Periods		60 seconds			
Velocity Readi	ng by Station:	(All velocity reading	igs in feet per sec	cond.)	
Station #	Point Velocity	Station #	Point Velocity	Station #	Point Velocity
A1	0.12	G1	0	L3	0.69
A2	0.27	G2	0.6	L4	0.8
A3	0.21	G3	0.83	L5	0.82
A4 A5	0.56	G5	0.76		0.78
AH1	0.1	G6	0.69	L8	0.86
AH2	-0.02	GH	0.84	LM	0.82
AB	0.36	H1	0.25	M1	0.04
B1 B2	0.03	H2 H3	0.66	M2 M3	0.14
B3	0.28	H4	0.82	M4	0.7
B4	0.38	H5	0.86	M5	0.8
B5 B6	0.43	H6	0.92	M6	0.8
B0 B7	0.3	HI	0.84	M8	0.91
B8	0.01	l1	0.02	MN	0.8
BC	0.69	12	0.06	N1	-0.06
C1	0.56	13	0.78	N2	0.14
C2 C3	0.85	14	0.75	N4	0.74
C4	0.85	16	0.83	N5	0.75
C5	0.96	17	0.82	N6	0.88
C6	0.75	18	0.8	N7	0.81
	0.86	IJ I1	0.71	N8 NO	0.68
D2	0.84	J2	0.00	01	0.36
D3	0.9	J3	0.76	O2	0.61
D4	0.92	J4	0.78	O3	0.76
D5	0.95	J5	0.83	04	0.81
DE	0.44	J7	0.89	OP	0.03
E1	0.11	J8	0.83	P1	0.43
E2	0.66	JK	0.78	P2	0.73
E3 E4	0.73	K1	0.39	P3 P4	0.8
E5	0.89	K3	0.65	P5	0.76
E6	0.82	K4	0.72	PQ	0.39
EF	0.91	K5	0.79	Q1	0.1
F1 F2	0.04	K6 K7	0.76	Q2	0.19
F3	0.04	K8	0.8	Q3	0.23
F4	0.94	KL	0.88	Q5	0.3
F5	0.85	L1	0.27	QH1	0.24
FG	0.91	L2	0.55	QH2	0.09

Table 1. Discharge of Mammoth Spring, Silver Springs Group, Marion County, Florida on September 10, 2007. Data record and calculation of discharge measurement.



Figure 1. Map of Mammoth Spring, Silver Springs Group, Marion County, Florida.



Figure 2. Discharge measurement cross-section; Mammoth Spring, Marion County, Florida, September 10, 2007 measurement. Cross-section is viewed to the upstream of observer, and is located between the 26- and 34-foot depth levels. Support poles are represented by dashed lines. Velocity measurement stations are shown as points along the support poles. See Table 1 for station velocities. Boundary wall of the cross section is shown as the perimeter ring of connected points. X- and Y-axis scales are shown in feet.

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Figure 3. Discharge measurement cross-section; Mammoth Spring, Marion County, Florida, September 10, 2007 measurement. Flow contour velocities are shown in feet per second. Areas with negative velocities (reverse flow) are shaded and delineated by hatched lines. Outer boundary of cross section represents the zero-value contour. X- and Y-axis scales are shown in feet.

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# TABLE 2. MAMMOTH SPRING, SEPTEMBER 10, 2007.SURFER 8 GRID VOLUME COMPUTATIONS AND GRIDDING REPORT

#### **UPPER SURFACE**

Grid File Name:	Y:\2. PROJECTS\KARST ENVIRONMENTAL\Silver Springs\Sep	
	07\Mammoth_9-07.bln.grd	
Grid Size:	61 rows x 356 columns	
X Minimum:	0	
X Maximum:	71	
X Spacing:	0.2	
Y Minimum:	0	
Y Maximum:	12	
Y Spacing:	0.2	
Z Minimum:	-0.034316339959011	
Z Maximum:	0.99097829840165	

### LOWER SURFACE

Level Surface defined by Z = 0

#### VOLUMES

Z Scale Factor:	1
Total Volumes by:	
Trapezoidal Rule:	207.77507328005
Simpson's Rule:	207.87237878945
Simpson's 3/8 Rule:	207.86180500243

#### **CUT & FILL VOLUMES**

Positive Volume [Cut]:207.78021158709Negative Volume [Fil]:0.0051383070426337Net Volume [Cut-Fil]:207.77507328005(The Net Volume value is used due to the presence of negative velocity values.Positive Vol. Cut - Negative Vol. Fill = Net Volume. Please refer to report text.)

#### AREAS

#### **Planar Areas**

#### **Operational Planar Area: 321.36 <<<< Total Cross-section Area in Square Feet**

(Calculated using blanking file due to the presence of negative velocity values;Operational Planar Area = [P.P.A.Cut + N.P.A.Fill] = [Total Planar Area - Blanked Planar Area].Please refer to report text.)Positive Planar Area [Cut]:320.87326059558Negative Planar Area [Fill]:0.48673940442225Blanked Planar Area:530.64Total Planar Area:852

## Surface Areas

Positive Surface Area [Cut]:	352.84575345995
Negative Surface Area [Fill]:	0.49183331134998

## **GRIDDING REPORT**

## **Data Source**

Source Data File Name:	Y:\2. PROJECTS\KARST ENVIRONMENTAL\Silver Springs\Sep	
	07\Mammoth 9-07 SURFER XYZ T3 750ptsBLF2.xls	
X Column:	A	
Y Column:	В	
Z Column:	C	
Data Counts		
Active Data:	750	
Original Data:	750	
Excluded Data:	0	
Deleted Duplicates:	0	
Retained Duplicates:	0	
Artificial Data:	0	
Superseded Data:	0	
<b>Univariate Statistics</b>		

	Х	Y	Z
Minimum:	0.5	1.4	-0.06
25%-tile: Median:	14.8 39	5.25 7 4	0
75%-tile:	59.3	9.05	0
Maximum:	70.8	10.7	0.96
Midrange:	35.65	6.05	0.45
Range:	70.3	9.3	1.02
Interquartile Range:	44.5	3.8	0
Median Abs. Deviation:	22	1.9	0
Mean:	37.107971826667	7.02198304	0.108
Trim Mean (10%):	37.268178801775	7.1205950887574	0.072233727810651
Standard Deviation:	23.059067233641	2.4236970117194	0.26369173922088
Variance:	531.72058168559	5.8743072046177	0.0695333333333333
Coef. of Variation: Coef. of Skewness:			2.4415901779711 2.2040540058234

# **Inter-Variable Correlation**

	Х	Y	Z	
X:	1.000	0.140	-0.048	
Y:		1.000	-0.026	
Z:			1.000	

Table 2. Mammoth Spring, September 10, 2007.

#### **Inter-Variable Covariance**

	Х	Y	Z
X: Y: Z:	531.72058168559	7.8064232576822 5.8743072046177	-0.28988762394667 -0.01651616832 0.069533333333333

## **Planar Regression: Z** = **AX**+**BY**+**C**

## **Fitted Parameters**

	А	В	С
Parameter Value:	-0.00051393670643368	-0.0021286188185886	0.14201827406578
Standard Error:	0.00042198513441429	0.0040147689826763	0.031772415802934

# **Inter-Parameter Correlations**

	A	В	С
A: B: C:	1.000	0.140 1.000	-0.369 0.818 1.000

## **ANOVA Table**

Source	df	Sum of Squares	Mean Square	F
Regression: Residual:	2 747	0.13810538803796 52.011894611962	0.069052694018	8982 0.99174 0471
Total:	749	52.15		

Coefficient of Multiple Determination (R^2): 0.0026482337111786

## **Nearest Neighbor Statistics**

	Separation	Delta Z
Minimum:	0.0499999999999999	0
25%-tile:	0.11661903789691	0
Median:	0.20396078054371	0
75%-tile:	0.40049968789001	0
Maximum:	2.0303940504247	0.91

Midrange:	1.0401970252123	0.455
Range:	1.9803940504247	0.91
Interquartile Range:	0.28388064999311	0
Median Abs. Deviation:	0.099557715454609	0
Mean:	0.31299595633224	0.058
Trim Mean (10%):	0.27102220218972	0.02207100591716
Standard Deviation:	0.30584150156674	0.17807938304775
Variance:	0.0935390240806	0.0317122666666667
Coef. of Variation:	0.97714202173941	3.0703341904784
Coef. of Skewness:	2.9410502101801	3.5343485345225
Root Mean Square:	0.43761340560012	0.18728658966052
Mean Square:	0.19150549276093	0.0350762666666667

## **Complete Spatial Randomness**

Lambda:	1.1471573441013
Clark and Evans:	0.67047133875302
Skellam:	1035.2502796423

# **Exclusion Filtering**

Exclusion Filter String: Not In Use

## **Duplicate Filtering**

Duplicate Points to Keep:	First
X Duplicate Tolerance:	8.3E-006
Y Duplicate Tolerance:	1.1E-006
No duplicate data were for	ınd.

#### **Breakline Filtering**

Breakline Filtering: Not In Use

## **Gridding Rules**

Gridding Method:	Kriging
Kriging Type:	Point

Polynomial Drift Order: 2 Kriging std. deviation grid: no

## **Semi-Variogram Model**

Component Type:	Linear
Anisotropy Angle:	0
Anisotropy Ratio:	3
Variogram Slope:	1

## **Search Parameters**

No Search (use all data): true

Table 2. Mammoth Spring, September 10, 2007.

# **Output Grid**

Grid File Name:	Y:\2. PROJECTS\KARST ENVIRONMENTAL\Silver Springs\Sep 07\Mammoth_9-07.grd
Grid Size:	61 rows x 356 columns
Total Nodes:	21716
Filled Nodes:	21716
Blanked Nodes:	0
Grid Geometry	
X Minimum:	0
X Maximum:	71
X Spacing:	0.2
Y Minimum:	0
Y Maximum:	12
Y Spacing:	0.2
Grid Statistics	
Z Minimum:	-3.6281612141484
Z 25%-tile:	-1.1764521731005
Z Median:	-0.25697093763238
Z 75%-tile:	0.59596069694474
Z Maximum:	0.99097829840165
Z Midrange:	-1.3185914578734
Z Range:	4.61913951255
Z Interquartile Range:	1.7724128700453
Z Median Abs. Deviation:	0.8834879030336
Z Mean:	-0.4238572527302
Z Trim Mean (10%):	-0.36894639109803
Z Standard Deviation:	1.0632967461044
Z Variance:	1.1305999702763
Z Coef. of Variation:	-1
Z Coef. of Skewness:	-0.56158676877364
Z Root Mean Square:	1.144663680287
Z Mean Square:	1.3102549409683



Figure 4. Discharge measurement cross-section; Mammoth Spring, Marion County, Florida, September 10, 2007 measurement. Relationship of flow contours (velocities shown in feet per second) and velocity measurement stations (labeled points) are shown. Areas with negative velocities (reverse flow) are shaded and delineated by hatched lines. See Table 1 for station velocities. Boundary wall of the cross section is shown as the perimeter ring of connected points. X- and Y-axis scales are shown in feet.

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Table 3. Mammoth Spring (Silver Springs Group) XYZ Grid Data, September 10, 2007.						
(Minor boundary points have been edited for processing in Surfer.)						
X	Y	Z (Velocity)	Station Name	X Plot	Y Plot	
67	6.75	0.12	A1	670	67.5	
67	7.5	0.27	A2	670	75	
67	8.5	0.21	A3	670	85	
67	9.5	0.38	A4	670	95	
67	9.75	0.54	A5	670	97.5	
68	8	0.1	AH1	680	80	
69	8	-0.02	AH2	690	80	
65	8	0.36	AB	650	80	
63	4.55	0.03	B1	630	45.5	
63	5.05	0.04	B2	630	50.5	
63	6.05	0.28	B3	630	60.5	
63	7.05	0.38	B4	630	70.5	
63	8.05	0.43	B5	630	80.5	
63	9.05	0.71	B6	630	90.5	
63	10.05	0.3	B7	630	100.5	
63	10.45	0.01	B8	630	104.5	
61	8	0.69	BC	610	80	
59	5.65	0.56	C1	590	56.5	
59	6.4	0.76	C2	590	64	
59	7.4	0.85	C3	590	74	
59	8.4	0.85	C4	590	84	
59	9.4	0.96	C5	590	94	
59	9.7	0.75	C6	590	97	
57	6.9	0.86	CD	570	69	
55	5.55	0.71	D1	550	55.5	
55	6.3	0.84	D2	550	63	
55	7.3	0.9	D3	550	73	
55	8.3	0.92	D4	550	83	
55	9.3	0.95	D5	550	93	
55	9.9	0.44	D6	550	99	
53	6.9	0.86	DE	530	69	
51	5.05	0.11	E1	510	50.5	
51	5.7	0.66	E2	510	57	
51	6.7	0.73	<b>E</b> 3	510	67	
51	7.8	0.78	E4	510	78	
51	8.7	0.89	E5	510	87	
51	9.4	0.82	E6	510	94	
49	7.7	0.91	EF	490	77	
47	5.55	0.04	<b>F</b> 1	470	55.5	
47	6.2	0.84	F2	470	62	

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
47	7.2	0.93	F3	470	72
47	8.2	0.94	F4	470	82
47	9	0.85	F5	470	90
45	7.7	0.91	FG	450	77
43	4.35	0	G1	430	43.5
43	5.1	0.6	G2	430	51
43	6.2	0.83	G3	430	62
43	7.1	0.76	G4	430	71
43	8.1	0.81	G5	430	81
43	8.6	0.69	G6	430	86
41	6.1	0.84	GH	410	61
39	3.75	0.25	H1	390	37.5
39	4.5	0.66	H2	390	45
39	5.5	0.81	H3	390	55
39	6.5	0.82	H4	390	65
39	7.5	0.86	H5	390	75
39	8.5	0.92	H6	390	85
39	9.3	0.86	H7	390	93
37	6.1	0.84	HI	370	61
35	2.7	0.02	l1	350	27
35	2.95	0.06	12	350	29.5
35	3.95	0.78	13	350	39.5
35	5.05	0.79	14	350	50.5
35	5.95	0.75	15	350	59.5
35	6.95	0.83	l6	350	69.5
35	7.95	0.82	17	350	79.5
35	8.75	0.8	18	350	87.5
33	4.95	0.71	IJ	330	49.5
31	2.1	0.08	J1	310	21
31	2.55	0.3	J2	310	25.5
31	3.55	0.76	J3	310	35.5
31	4.55	0.78	J4	310	45.5
31	5.55	0.83	Jo	310	55.5
31	0.00	0.89	J6	310	05.5 75.5
31	7.55	0.86	J7	310	75.5
31	8.35	0.83	J8	310	83.5
29	4.90	U./ð	JN	290	49.0
	1 55	0.20	<b>K</b> 1	270	15 5
21	2.2	0.59	K2	270	10.0
21	2.3	0.55	K2 K2	270	23
27	4.3	0.72	K4	270	43
27	5.3	0.79	K5	270	53
27	6.4	0.76	K6	270	64

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
27	7.3	0.87	K7	270	73
27	8.2	0.8	K8	270	82
25	6.3	0.88	KL	250	63
23	1.95	0.27	L1	230	19.5
23	2.2	0.55	L2	230	22
23	3.2	0.69	L3	230	32
23	4.2	0.8	L4	230	42
23	5.2	0.82	L5	230	52
23	6.2	0.78	L6	230	62
23	7.2	0.87	L7	230	72
23	8.1	0.86	L8	230	81
21	6.3	0.82	LM	210	63
10	0.05	0.04	N44	400	00 F
19	2.30	0.04	IVI 1 MO	190	23.0
19	2.0	0.14	M2	190	20
19	J.0 / A	0.03	IVIJ MA	130	30
19	4.0	0.7	M4 M5	190	40
19	6.6	0.0	MG	190	66
19	7.6	0.0	M7	190	76
19	8.2	0.91	M8	190	82
17	7.1	0.8	MN	170	71
15	3.35	-0.06	N1	150	33.5
15	3.85	0.14	N2	150	38.5
15	4.85	0.71	N3	150	48.5
15	5.85	0.74	N4	150	58.5
15	6.85	0.75	N5	150	68.5
15	7.85	0.88	N6	150	78.5
15	8.85	0.81	N7	150	88.5
15	9.05	0.68	N8	150	90.5
13	7.1	0.82	NO	130	71
		0.02			
11	5.25	0.36	01	110	52.5
11	6	0.61	02	110	60
11	7	0.76	03	110	70
11	8	0.81	04	110	80
11	8.6	0.63	05	110	86
9	7.5	0.77	OP	90	75
			0.		
7	67	0 43	P1	70	67
7	72	0.73	P2	70	72
7	8.2	0.8	P3	70	82
7	9.2	0.82	P4	70	92
7	9.2	0.02	P5	70	92
5	7.5	0.70	PO	50	75
5	1.5	0.33	1.64	50	15
2	6	01	01	30	60
3	U	0.1	<b>V</b> I	50	00

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
3	6.5	0.19	Q2	30	65
3	7.4	0.23	Q3	30	74
3	7.7	0.3	Q4	30	77
3	8.3	0.3	Q5	30	83
2.5	7.5	0.24	QH1	25	75
2	7.5	0.09	QH2	20	75
70.1	8	0	AE	701	80
70	7.85	0	AESA	700	78.5
69.5	7.75	0	AESB	695	77.5
69	7.55	0	AESC	690	75.5
68.75	7.5	0	AESD	687.5	75
68.5	7.35	0	AESE	685	73.5
68.5	7.25	0	AESF	685	72.5
68	7.1	0	AESG	680	71
67.75	7	0	AESH	677.5	70
67.5	6.75	0	AESI	675	67.5
67.45	6.75	0	AESJ	674.5	67.5
67	6.6	0	AS	670	66
66.5	6.3	0	ABSA	665	63
66	6.85	0	ABSB	660	68.5
65.5	6.85	0	ABSC	655	68.5
65	6.95	0	ABS	650	69.5
64.5	6.9	0	ABSD	645	69
64	6.8	0	ABSE	640	68
63.9	6.75	0	ABSF	639	67.5
63.9	6.55	0	ABSG	639	65.5
63.9	6.3	0	ABSH	639	63
63.9	6.05	0	ABSI	639	60.5
63.9	5.8	0	ABSJ	639	58
63.8	5.55	0	ABSK	638	55.5
63.8	5.3	0	ABSL	638	53
63.85	5.05	0	ABSM	638.5	50.5
63.8	4.8	0	ABSN	638	48
63.7	4.55	0	ABSO	637	45.5
63.5	4	0	ABSP	635	40
63	4.35	0	BS	630	43.5
62.4	4.55	0	BCSA	624	45.5
62.65	4.8	0	BCSB	626.5	48
62.75	5.05	0	BCSC	627.5	50.5
62.65	5.15	0	BCSD	626.5	51.5
62.5	5.1	0	BCSE	625	51
62	5.35	0	BCSF	620	53.5
61.5	4.95	0	BCSG	615	49.5
61	5.9	0	BCS	610	59
60.5	5.2	0	BCSH	605	52
60	5.2	0	BCSI	600	52
59.5	5.45	0	BCSJ	595	54.5

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
59	5.4	0	CS	590	54
58.5	4.45	0	CDSA	585	44.5
58	4.9	0	CDSB	580	49
57.5	5.15	0	CDSC	575	51.5
57	5.4	0	CDS	570	54
56.5	5.15	0	CDSD	565	51.5
56	5.05	0	CDSE	560	50.5
55.5	5.4	0	CDSF	555	54
55	5.3	0	DS	550	53
53	5.1	0	DES	530	51
51	4.9	0	ES	510	49
49	5.7	0	EFS	490	57
47	5.4	0	FS	470	54
45	4.95	0	FGS	450	49.5
43	4.2	0	GS	430	42
41	4.1	0	GHS	410	41
39	3.6	0	HS	390	36
37	3.3	0	HIS	370	33
35	2.45	0	IS	350	24.5
33	2.35	0	IJS	330	23.5
31	1.95	0	JS	310	19.5
29	2.05	0	JKS	290	20.5
27	1.4	0	KS	270	14
25	1.5	0	KLS	250	15
23	1.7	0	LS	230	17
21	2.1	0	LMS	210	21
19	2.1	0	MS	190	21
17	3.05	0	MNS	170	30.5
15	3.15	0	NS	150	31.5
13	4.3	0	NOS	130	43
11	5.1	0	OS	110	51
10.5	5.45	0	OPSA	105	54.5
10	5.7	0	OPSB	100	57
9.5	5.85	0	OPSC	95	58.5
9	6.05	0	OPS	90	60.5
8.5	6.25	0	OPSD	85	62.5
8	6.4	0	OPSE	80	64
7.5	6.5	0	OPSF	75	65
1	6.5	0	PS	70	65
6.5	6.55	0	PQSA	65	65.5
6	0.0 6.05	U	PQSB	6U	66 F
5.5 <i>F</i>	C0.0	0	P436	50	C.00
<b>5</b>	0.0	U	ruð Doed	5U 45	00
4.5	0.40	0	PQSD	40	04.5
4		0	POSE	4U 25	02 50 5
3.0 2	5.95	0	<u>ru</u> 3r 09	30 20	59.0 50
ی ۲	J.0 E 0E	0	43	3U 25	00 50 5
2.3	5.65	U	<b>USA</b>	20	<b>30.</b> 3

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
2.1	6	0	QSB	21	60
2	6	0	QSC	20	60
1.8	6.25	0	QSD	18	62.5
1.7	6.3	0	QSE	17	63
1.7	6.5	0	QSF	17	65
1.6	6.75	0	QSG	16	67.5
1.5	7	0	QSH	15	70
1.6	7.25	0	QSI	16	72.5
1.7	7.5	0	QE	17	75
1.85	7.75	0	QTF	18.5	77.5
0.5	8	0	QTE	5	80
1.7	8.25	0	QTD	17	82.5
1.8	8.25	0	QTC	18	82.5
2	8.35	0	QTB	20	83.5
2.5	8.45	0	QTA	25	84.5
3	8.5	0	QT	30	85
3.5	8.6	0	PQTF	35	86
4	8.65	0	PQTE	40	86.5
4.5	9	0	PQTD	45	90
5	8.85	0	PQT	50	88.5
5.5	9.05	0	PQTC	55	90.5
6	9.4	0	PQTB	60	94
6.5	9.55	0	ΡQTA	65	95.5
7	9.65	0	PT	70	96.5
7.5	9.7	0	OPTJ	75	97
8	9.75	0	OPTI	80	97.5
8.55	9.45	0	OPTH	85.5	94.5
8.5	9.2	0	OPTG	85	92
8.5	8.95	0	OPTF	85	89.5
8.5	8.7	0	OPTE	85	87
8.5	8.6	0	OPTD	85	86
9	8.55	0	OPT	90	85.5
9.5	8.55	0	OPTC	95	85.5
10	8.75	0	OPTB	100	87.5
10.5	8.85	0	ΟΡΤΑ	105	88.5
11	8.75	0	ОТ	110	87.5
13	8.55	0	NOT	130	85.5
15	9.15	0	NT	150	91.5
17	9.4	0	MNT	170	94
19	8.4	0	MT	190	84
21	8.4	0	LMT	210	84
23	8.4	0	LT	230	84
25	8.4	0	KLT	250	84
27	8.4	0	КТ	270	84
29	8.55	0	JKT	290	85.5
31	8.55	0	JT	310	85.5
33	8.95	0	IJT	330	89.5
35	9.05	0	IT	350	90.5

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
37	9.4	0	HIT	370	94
39	9.5	0	HT	390	95
41	9.4	0	GHT	410	94
43	8.8	0	GT	430	88
45	9.25	0	FGT	450	92.5
47	9.3	0	FT	470	93
49	9.55	0	EFT	490	95.5
51	9.7	0	ET	510	97
53	9.95	0	DET	530	99.5
55	10.2	0	DT	550	102
55.5	10.1	0	CDTF	555	101
56	9.95	0	CDTE	560	99.5
56.5	9.95	0	CDTD	565	99.5
57	9.95	0	CDT	570	99.5
57.5	10	0	CDTC	575	100
58	10.05	0	CDTB	580	100.5
58.5	10	0	CDTA	585	100
59	9.95	0	СТ	590	99.5
59.5	9.95	0	BCTF	595	99.5
60	9.8	0	BCTE	600	98
60.5	9.85	0	BCTD	605	98.5
61	9.85	0	BCT	610	98.5
61.5	10.1	0	BCTC	615	101
62	10.4	0	BCTB	620	104
62.5	10.7	0	BCTA	625	107
63	10.7	0	BT	630	107
63.5	10.65	0	ABTF	635	106.5
64	10.45	0	ABTE	640	104.5
64.5	10.4	0	ABTD	645	104
65	10.4	0	ABT	650	104
65.5	10.5	0	ABTC	655	105
66	10.45	0	ABTB	660	104.5
66.5	10.2	0	ABTA	665	102
67	10	0	AT	670	100
67.5	9.9	0	AETM	675	99
67.7	9.75	0	AETL	677	97.5
68	9.6	0	AETK	680	96
68.2	9.5	0	AETJ	682	95
68.5	9.4	0	AETI	685	94
69	9.35	0	AETH	690	93.5
69.4	9.25	0	AETG	694	92.5
69.5	9.1	0	AETF	695	91
70.4	9	0	AETE	704	90
70.8	8.75	0	AETD	708	87.5
69.6	8.5	0	AETC	696	85
69.75	8.25	0	AETB	697.5	82.5
70	8.2	0	AETA	700	82

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
	7.00	•	45044		70.0
69.9	7.83	0	AESAI	699	78.3
69.7	7.79	0	AESA3	697	77.9
60.4	7 74	•		604	77.4
69.4 60.2	7.71	0	AESDI	694	70.0
69.2	7.63	0	AESB3	692	/6.3
68.9	7 53	0	AFSC1	689	75.3
		•			
68.6	7.38	0	AESD2	686	73.8
68.4	7.22	0	AESF1	684	72.2
68.2	7.16	0	AESF3	682	71.6
67.9	7.06	0	AESG1	679	70.6
67.6	6.8	0	AESH2	676	68
67.3	6.69	0	AESJ2	673	66.9
67.1	6.63	0	AESJ4	671	66.3
66.9	6.54	0	AS1	669	65.4
66.7	6.42	0	AS3	667	64.2
66.3182	6.5	0	ABSA2	663.182	65
66.2273	6.6	0	ABSA3	662.273	66
66.1364	6.7	0	ABSA4	661.364	67
66.0445	6.8	0	ABSA5	660.445	68
05.0	0.05	•	45050	050	00.5
65.8	6.85	0	ABSB2	658	68.5
65.6	6.85	0	ABSB4	656	68.5
65.3	6.89	0	ABSC2	653	68.9
65.1	6.93	0	ABSC4	651	69.3
		-			
64.9	6.94	0	ABS1	649	69.4
64.7	6.92	0	ABS3	647	69.2
64.4	6.88	0	ABSD1	644	68.8
64.2	6.84	0	ABSD3	642	68.4
63.6385	4.4	0	ABSO2	636.3848	44
63.577	4.2	0	ABSO4	635.7696	42
63.3	4.14	0	ABSP2	633	41.4
63.1	4.28	0	ABSP4	631	42.8
62.8	4.41666	0	BS2	628	44.1666

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
62.6	4.48332	0	BS4	626	44.8332
62.525	4.675	0	BCSA1	625.25	46.75
62.7	4.9	0	BCSB1	627	49
62.4	5.15	0	BCSE1	624	51.5
62.2	5.25	0	BCSE3	622	52.5
61.8	5.21	0	BCSF2	618	52.1
61.6	5.07	0	BCSF4	616	50.7
61.3947	5.2	0	BCSG2	613.9474	52
61.2895	5.4	0	BCSG4	612.8949	54
61.1842	5.6	0	BCSG6	611.8422	56
61.079	5.8	0	BCSG8	610.7896	58
60.9286	5.8	0	BCS1	609.2858	58
60.7857	5.6	0	BCS3	607.8574	56
60.6429	5.4	0	BSC5	606.429	54
60.4	5.2	0	BCSH1	604	52
60.2	5.2	0	BCSH3	602	52
59.8	5.3	0	BCSI2	598	53
59.6	5.4	0	BCSI4	596	54
59.3	5.43	0	BCSJ2	593	54.3
59.1	5.41	0	BCSJ4	591	54.1
58.8947	5.2	0	CS2	588.9474	52
58.7895	5	0	CS4	587.8948	50
58.6842	4.8	0	CS6	586.8422	48
58.579	4.6	0	CS8	585.7896	46
58.4	4.54	0	CDSA1	584	45.4
58.2	4.72	0	CDSA3	582	47.2
57.9	4.95	0	CDSB1	579	49.5
57.7	5.05	0	CDSB3	577	50.5
57.3	5.25	0	CDSC2	573	52.5
57.1	5.35	0	CDSC4	571	53.5
56.9	5.35	0	CDS1	569	53.5
56.7	5.25	0	CDS3	567	52.5
56.4	5.13	0	CDSD1	564	51.3

56.2 $5.09$ $0$ CDSD3 $562$ $50.9$ $55.8$ $5.19$ $0$ CDSE2 $558$ $51.9$ $55.6$ $5.33$ $0$ CDSE4 $556$ $53.3$ $55.3$ $5.36$ $0$ CDSF2 $553$ $53.6$ $55.1$ $5.32$ $0$ CDSF4 $551$ $53.2$ $54.6$ $5.26$ $0$ DS4 $542$ $52.2$ $53.8$ $5.18$ $0$ DS12 $538$ $51.8$ $53.4$ $5.14$ $0$ DS16 $534$ $51.4$ $52.6$ $5.06$ $0$ DES4 $526$ $50.6$ $52.2$ $5.02$ $0$ DES4 $522$ $50.2$ $51.4$ $4.94$ $0$ DES12 $518$ $49.8$ $51.4$ $4.94$ $0$ ES2 $508$ $49.8$ $50.4$ $5.14$ $0$ ES6 $504$ $51.4$	X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
55.8         5.19         0         CDSE2         55.8         51.9           55.6         5.33         0         CDSE4         556         53.3           55.3         5.36         0         CDSF2         553         53.6           55.1         5.32         0         CDSF4         551         53.2           54.6         5.26         0         DS4         546         52.6           54.2         5.22         0         DS8         542         52.2           53.8         5.18         0         DS12         538         51.4           52.6         5.06         0         DES4         526         50.6           52.2         5.02         0         DES8         522         50.2           51.8         4.98         0         DES12         518         49.8           51.4         4.94         0         DES16         514         49.4           50.8         4.98         0         ES2         508         49.8           50.4         5.14         0         ES6         504         51.4           49.2         5.62         0         ES18         492         56	56.2	5.09	0	CDSD3	562	50.9
55.8         5.19         0         CDSE2         558         51.9           55.6         5.33         0         CDSE4         556         53.3           55.3         5.36         0         CDSF2         553         53.6           55.1         5.32         0         CDSF4         551         53.2           54.6         5.26         0         DS4         546         52.6           54.2         5.22         0         DS8         542         52.2           53.8         5.18         0         DS12         538         51.4           52.6         5.06         0         DES4         526         50.6           52.2         5.02         0         DES8         522         50.2           51.8         4.98         0         DES12         518         49.8           51.4         4.94         0         DES16         514         49.4           50.8         4.98         0         ES2         508         49.8           50.4         5.14         0         ES6         504         51.4           49.6         5.46         0         ES14         496         54.						
55.6 $5.33$ 0         CDSE4 $556$ $53.3$ $55.3$ $5.36$ 0         CDSF2 $553$ $53.6$ $55.1$ $5.32$ 0         CDSF4 $551$ $53.2$ $54.6$ $5.26$ 0         DS4 $542$ $52.2$ $53.8$ $5.18$ 0         DS12 $538$ $51.4$ $53.4$ $5.14$ 0         DS16 $534$ $51.4$ $52.6$ $5.06$ 0         DES4 $522$ $50.2$ $51.8$ $4.98$ 0         DES12 $518$ $49.8$ $51.4$ $4.98$ 0         DES16 $514$ $49.4$ $$	55.8	5.19	0	CDSE2	558	51.9
55.3         5.36         0         CDSF2         553         53.6           55.1         5.32         0         CDSF4         551         53.2           54.6         5.26         0         DS4         546         52.6           54.2         5.22         0         DS8         542         52.2           53.8         5.18         0         DS12         538         51.8           52.6         5.06         0         DES4         526         50.6           52.2         5.02         0         DES8         522         50.2           51.8         4.98         0         DES12         518         49.8           51.4         4.94         0         DES12         518         49.8           51.4         4.94         0         DES12         518         49.8           50.4         5.14         0         ES6         504         51.4           49.6         5.46         0         ES14         496         54.6           49.2         5.62         0         ES18         492         56.2           448.8         5.67         0         EFS18         472         5	55.6	5.33	0	CDSE4	556	53.3
55.3 $5.36$ 0         CDSF2 $553$ $53.6$ $55.1$ $5.32$ 0         CDSF4 $551$ $53.2$ $54.6$ $5.26$ 0         DS4 $546$ $52.6$ $54.2$ $5.22$ 0         DS8 $542$ $52.2$ $53.8$ $5.18$ 0         DS16 $534$ $51.4$ $52.6$ $5.06$ 0         DES4 $526$ $50.6$ $52.2$ $5.02$ 0         DES4 $522$ $50.2$ $51.8$ $4.98$ 0         DES12 $518$ $49.8$ $51.4$ $4.94$ 0         DES16 $514$ $49.4$ $50.3$ $4.98$ 0         ES2 $508$ $49.8$ $50.4$ $5.14$ 0         ES6 $504$ $51.4$ $50.4$ $5.46$ 0         ES18 $492$ $56.2$ $48.8$ $5.67$ 0         EFS2 $488$ $56.7$ $48.4$ <						
55.1 $5.32$ 0         CDSF4 $551$ $53.2$ $54.6$ $5.26$ 0         DS4 $546$ $52.6$ $54.2$ $5.22$ 0         DS8 $542$ $52.2$ $53.8$ $5.18$ 0         DS12 $538$ $51.4$ $53.4$ $5.14$ 0         DS16 $534$ $51.4$ $52.6$ $5.06$ 0         DES4 $526$ $50.6$ $52.2$ $5.02$ 0         DES8 $522$ $50.2$ $51.8$ $4.98$ 0         DES16 $514$ $49.8$ $51.4$ $4.98$ 0         DES16 $514$ $49.8$ $50.4$ $5.14$ 0         ES6 $504$ $51.4$ $50$ $5.3$ 0         ES10 $500$ $53$ $49.6$ $5.46$ 0         EF814 $496$ $54.6$ $49.2$ $5.62$ 0         EF814 $476$ $54.9$ $448.4$ <td>55.3</td> <td>5.36</td> <td>0</td> <td>CDSF2</td> <td>553</td> <td>53.6</td>	55.3	5.36	0	CDSF2	553	53.6
54.6         5.26         0         DS4         546         52.6           54.2         5.22         0         DS8         542         52.2           53.8         5.18         0         DS12         538         51.8           53.4         5.14         0         DS16         534         51.4           52.6         5.06         0         DES4         526         50.6           52.2         5.02         0         DES8         522         50.2           51.8         4.98         0         DES12         518         49.8           51.4         4.94         0         DES16         514         49.4           50.8         4.98         0         ES2         508         49.8           50.4         5.14         0         ES6         504         51.4           49.6         5.46         0         ES10         500         53           49.6         5.62         0         ES18         492         56.2           48.8         5.67         0         EFS2         488         56.7           48.8         5.55         0         EFS14         476         54.9 <td>55.1</td> <td>5.32</td> <td>0</td> <td>CDSF4</td> <td>551</td> <td>53.2</td>	55.1	5.32	0	CDSF4	551	53.2
54.6         5.26         0         DS4         546         52.6           54.2         5.22         0         DS8         542         52.2           53.8         5.18         0         DS12         538         51.8           53.4         5.14         0         DS16         534         51.4           52.6         5.06         0         DES8         522         50.2           51.8         4.98         0         DES12         518         49.8           51.4         4.94         0         DES12         518         49.8           51.4         4.94         0         DES16         514         49.4           50.8         4.98         0         ES2         508         49.8           50.4         5.14         0         ES6         504         51.4           49.6         5.46         0         ES14         496         54.6           48.8         5.67         0         EFS2         488         56.7           48.8         5.67         0         EFS2         488         56.7           48.8         5.67         0         EFS2         488         56.7 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>						
54.2         5.22         0         DS8         542         52.2           53.8         5.18         0         DS12         538         51.8           53.4         5.14         0         DS16         534         51.4           52.6         5.06         0         DES4         526         50.6           52.2         5.02         0         DES8         522         50.2           51.8         4.98         0         DES12         518         49.8           51.4         4.94         0         DES12         518         49.8           50.4         5.14         0         ES6         504         51.4           49.6         5.46         0         ES10         500         53           49.6         5.46         0         ES14         496         54.6           49.2         5.62         0         ES18         492         56.2           48.8         5.67         0         EFS2         488         56.7           48.4         5.61         0         EFS14         476         54.9           47.6         5.49         0         EFS18         472         54.3<	54.6	5.26	0	DS4	546	52.6
53.8       5.18       0       DS12       538       51.8         53.4       5.14       0       DS16       534       51.4         52.6       5.06       0       DES4       526       50.6         52.2       5.02       0       DES8       522       50.2         51.8       4.98       0       DES12       518       49.8         51.4       4.94       0       DES16       514       49.4         50.8       4.98       0       ES2       508       49.8         50.4       5.14       0       ES6       504       51.4         49.6       5.46       0       ES10       500       53         49.6       5.46       0       ES14       496       54.6         49.2       5.62       0       EFS2       488       56.7         48.8       5.67       0       EFS2       488       56.7         48.8       5.67       0       EFS14       476       54.9         47.2       5.43       0       EFS14       476       54.9         47.2       5.43       0       FS10       480       55.5	54.2	5.22	0	DS8	542	52.2
53.4       5.14       0       DS16       534       51.4         52.6       5.06       0       DES4       526       50.6         52.2       5.02       0       DES8       522       50.2         51.8       4.98       0       DES12       518       49.8         51.4       4.94       0       DES16       514       49.4	53.8	5.18	0	DS12	538	51.8
52.6         5.06         0         DES4         526         50.6           52.2         5.02         0         DES8         522         50.2           51.8         4.98         0         DES12         518         49.8           51.4         4.94         0         DES16         514         49.4           50.8         4.98         0         ES2         508         49.8           50.4         5.14         0         ES6         504         51.4           50         5.3         0         ES10         500         53           49.6         5.46         0         ES14         496         54.6           49.2         5.62         0         ES18         492         56.2	53.4	5.14	0	DS16	534	51.4
52.6         5.06         0         DES4         526         50.6           52.2         5.02         0         DES8         522         50.2           51.8         4.98         0         DES12         518         49.8           51.4         4.94         0         DES16         514         49.4           50.8         4.98         0         ES2         508         49.8           50.4         5.14         0         ES6         504         51.4           50         5.3         0         ES10         500         53           49.6         5.46         0         ES14         496         54.6           49.2         5.62         0         ES18         492         56.2		_				
52.2         5.02         0         DES8         522         50.2           51.8         4.98         0         DES12         518         49.8           51.4         4.94         0         DES16         514         49.4           50.8         4.98         0         ES2         508         49.8           50.4         5.14         0         ES6         504         51.4           50         5.3         0         ES10         500         53           49.6         5.46         0         ES14         496         54.6           49.2         5.62         0         ES18         492         56.2	52.6	5.06	0	DES4	526	50.6
51.8         4.98         0         DES12         518         49.8           51.4         4.94         0         DES16         514         49.4           50.8         4.98         0         ES2         508         49.4           50.4         5.14         0         ES6         504         51.4           50         5.3         0         ES10         500         53           49.6         5.46         0         ES14         496         54.6           49.2         5.62         0         ES18         492         56.2	52.2	5.02	0	DES8	522	50.2
51.4         4.94         0         DES16         514         49.4           50.8         4.98         0         ES2         508         49.8           50.4         5.14         0         ES6         504         51.4           50         5.3         0         ES10         500         53           49.6         5.46         0         ES14         496         54.6           49.2         5.62         0         ES18         492         56.2           48.8         5.67         0         EFS2         488         56.7           48.4         5.61         0         EFS10         480         55.5           47.6         5.49         0         EFS10         480         55.5           47.2         5.43         0         EFS18         472         54.3           46.8         5.355         0         FS2         468         53.55           46.4         5.265         0         FS6         464         52.65           46         5.175         0         FS10         460         51.75           45.6         5.085         0         FS14         456         50.85	51.8	4.98	0	DES12	518	49.8
50.8         4.98         0         ES2         508         49.8           50.4         5.14         0         ES6         504         51.4           50         5.3         0         ES10         500         53           49.6         5.46         0         ES14         496         54.6           49.2         5.62         0         ES18         492         56.2           48.8         5.67         0         EFS2         488         56.7           48.4         5.61         0         EFS2         488         56.7           48.4         5.61         0         EFS10         480         55.5           47.6         5.49         0         EFS14         476         54.9           47.2         5.43         0         EFS18         472         54.3           5.65         0         FS2         468         53.55         55           46.8         5.355         0         FS10         460         51.75           46.4         5.265         0         FS6         464         52.65           46         5.175         0         FS14         456         50.85 <td>51.4</td> <td>4.94</td> <td>0</td> <td>DES16</td> <td>514</td> <td>49.4</td>	51.4	4.94	0	DES16	514	49.4
50.8 $4.98$ 0       ES2 $508$ $49.8$ $50.4$ $5.14$ 0       ES6 $504$ $51.4$ $50$ $5.3$ 0       ES10 $500$ $53$ $49.6$ $5.46$ 0       ES14 $496$ $54.6$ $49.2$ $5.62$ 0       ES18 $492$ $56.2$ 48.8 $5.67$ 0       EFS2 $488$ $56.7$ $48.4$ $5.61$ 0       EFS6 $484$ $56.1$ $48$ $5.55$ 0       EFS10 $480$ $55.5$ $47.6$ $5.49$ 0       EFS14 $476$ $54.9$ $47.2$ $5.43$ 0       EFS18 $472$ $54.3$ $46.8$ $5.355$ 0       FS2 $468$ $53.55$ $46.4$ $5.265$ 0       FS10 $460$ $51.75$ $45.6$ $5.085$ 0       FS14 $456$ $50.85$ $45.2$ $4.995$ 0       FS18 $452$ $49.95$ $44.8$						
50.4 $5.14$ 0         ES6 $504$ $51.4$ $50$ $5.3$ 0         ES10 $500$ $53$ $49.6$ $5.46$ 0         ES14 $496$ $54.6$ $49.2$ $5.62$ 0         ES18 $492$ $56.2$ $48.8$ $5.67$ 0         EFS2 $488$ $56.7$ $48.4$ $5.61$ 0         EFS2 $488$ $56.7$ $48.4$ $5.61$ 0         EFS6 $484$ $56.1$ $48$ $5.55$ 0         EFS10 $480$ $55.5$ $47.6$ $5.49$ 0         EFS14 $476$ $54.9$ $47.2$ $5.43$ 0         EFS18 $472$ $54.3$ $47.2$ $5.43$ 0         EFS18 $472$ $54.3$ $46.8$ $5.355$ 0         FS2 $468$ $53.55$ $46.4$ $5.265$ 0         FS14 $456$ $50.85$ $45.2$ </td <td>50.8</td> <td>4.98</td> <td>0</td> <td>ES2</td> <td>508</td> <td>49.8</td>	50.8	4.98	0	ES2	508	49.8
50         5.3         0         ES10         500         53           49.6         5.46         0         ES14         496         54.6           49.2         5.62         0         ES18         492         56.2           48.8         5.67         0         EFS2         488         56.7           48.4         5.61         0         EFS2         488         56.7           48.4         5.61         0         EFS6         484         56.1           48         5.55         0         EFS10         480         55.5           47.6         5.49         0         EFS18         472         54.3	50.4	5.14	0	ES6	504	51.4
49.6       5.46       0       ES14       496       54.6         49.2       5.62       0       ES18       492       56.2         48.8       5.67       0       EFS2       488       56.7         48.4       5.61       0       EFS6       484       56.1         48       5.55       0       EFS10       480       55.5         47.6       5.49       0       EFS14       476       54.9         47.2       5.43       0       EFS18       472       54.3         46.8       5.355       0       FS2       468       53.55         46.4       5.265       0       FS6       464       52.65         46       5.175       0       FS10       460       51.75         45.6       5.085       0       FS14       456       50.85         44.8       4.874       0       FGS2       448       48.74         44.8       4.874       0       FGS2       448       48.74         44.4       4.722       0       FGS6       444       47.22         44.4       4.57       0       FGS10       440       45.7 </td <td>50</td> <td>5.3</td> <td>0</td> <td>ES10</td> <td>500</td> <td>53</td>	50	5.3	0	ES10	500	53
49.2       5.62       0       ES18       492       56.2         48.8       5.67       0       EFS2       488       56.7         48.4       5.61       0       EFS6       484       56.1         48       5.55       0       EFS10       480       55.5         47.6       5.49       0       EFS14       476       54.9         47.2       5.43       0       EFS18       472       54.3         46.8       5.355       0       FS2       468       53.55         46.4       5.265       0       FS1       464       52.65         46       5.175       0       FS1       460       51.75         45.6       5.085       0       FS14       456       50.85         45.2       4.995       0       FGS2       448       48.74         44.8       4.874       0       FGS2       448       48.74         44.4       4.722       0       FGS10       440       45.7         44.4       4.722       0       FGS10       444       47.22         44       4.57       0       FGS10       440       45.7 </td <td>49.6</td> <td>5.46</td> <td>0</td> <td>ES14</td> <td>496</td> <td>54.6</td>	49.6	5.46	0	ES14	496	54.6
48.8       5.67       0       EFS2       488       56.7         48.4       5.61       0       EFS6       484       56.1         48       5.55       0       EFS10       480       55.5         47.6       5.49       0       EFS14       476       54.9         47.2       5.43       0       EFS18       472       54.3         46.8       5.355       0       FS2       468       53.55         46.4       5.265       0       FS6       464       52.65         46       5.175       0       FS10       460       51.75         45.6       5.085       0       FS18       452       49.95         44.8       4.874       0       FGS2       448       48.74         44.8       4.874       0       FGS2       448       48.74         44.4       4.722       0       FGS10       440       45.7         43.8       4.874       0       FGS12       438       44.94         43.4       4.342       0       FGS16       434       43.42         42.6       4.18       0       GS4       426       41.8	49.2	5.62	0	ES18	492	56.2
48.8       5.67       0       EFS2       488       56.7         48.4       5.61       0       EFS6       484       56.1         48       5.55       0       EFS10       480       55.5         47.6       5.49       0       EFS14       476       54.9         47.2       5.43       0       EFS18       472       54.3         46.8       5.355       0       FS2       468       53.55         46.4       5.265       0       FS6       464       52.65         46       5.175       0       FS10       460       51.75         45.6       5.085       0       FS14       456       50.85         45.2       4.995       0       FS18       452       49.95         44.8       4.874       0       FGS2       448       48.74         44.4       4.722       0       FGS10       440       45.7         43.8       4.874       0       FGS12       438       44.94         43.4       4.342       0       FGS16       434       43.42         42.6       4.18       0       GS4       426       41.8	40.0	5.07		5500	400	50.7
46.4       5.61       0       EFS0       464       36.1         48       5.55       0       EFS10       480       55.5         47.6       5.49       0       EFS14       476       54.9         47.2       5.43       0       EFS18       472       54.3         46.8       5.355       0       FS2       468       53.55         46.4       5.265       0       FS2       468       53.55         46.4       5.265       0       FS10       460       51.75         46.6       5.175       0       FS10       460       51.75         45.6       5.085       0       FS14       456       50.85         45.2       4.995       0       FGS2       448       48.74         44.8       4.874       0       FGS2       448       48.74         44.4       4.722       0       FGS10       440       45.7         43.8       4.874       0       FGS12       438       44.94         44.4       4.57       0       FGS12       438       44.94         43.4       4.342       0       FGS16       434       43.42<	48.8	5.67	0	EFS2	488	56.7
46       5.35       0       EFS10       460       53.3         47.6       5.49       0       EFS14       476       54.9         47.2       5.43       0       EFS18       472       54.3         46.8       5.355       0       FS2       468       53.55         46.4       5.265       0       FS6       464       52.65         46       5.175       0       FS10       460       51.75         45.6       5.085       0       FS14       456       50.85         45.2       4.995       0       FS18       452       49.95         44.8       4.874       0       FGS2       448       48.74         44.4       4.722       0       FGS6       444       47.22         44.4       4.57       0       FGS10       440       45.7         43.8       4.494       0       FGS12       438       44.94         43.4       4.342       0       FGS16       434       43.42         42.6       4.18       0       GS4       426       41.8         42.6       4.18       0       GS8       422       41.6	40.4	5.01	0	EF30 EES10	404	56.1
47.0 $3.43$ 0       EF314       476 $34.3$ 47.2 $5.43$ 0       EFS18       472 $54.3$ 46.8 $5.355$ 0       FS2       468 $53.55$ 46.4 $5.265$ 0       FS6       464 $52.65$ 46 $5.175$ 0       FS10       460 $51.75$ 45.6 $5.085$ 0       FS14       456 $50.85$ 45.2 $4.995$ 0       FS18 $452$ $49.95$ 44.8 $4.874$ 0       FGS2 $448$ $48.74$ 44.4 $4.72$ 0       FGS2 $448$ $48.74$ 44.8 $4.874$ 0       FGS2 $448$ $48.74$ 44.4 $4.72$ 0       FGS10 $444$ $47.22$ 44 $4.57$ 0       FGS10 $444$ $47.22$ 44 $4.57$ 0       FGS12 $438$ $44.94$ 43.4 $4.342$ 0       FGS16 $434$ $43.42$ 42.6 $4.18$	40	5.55	0	EFS10 EES14	400	53.5
47.2 $3.43$ $0$ $EFS16$ $472$ $34.3$ $46.8$ $5.355$ $0$ $FS2$ $468$ $53.55$ $46.4$ $5.265$ $0$ $FS6$ $464$ $52.65$ $46$ $5.175$ $0$ $FS10$ $460$ $51.75$ $45.6$ $5.085$ $0$ $FS14$ $456$ $50.85$ $45.2$ $4.995$ $0$ $FS18$ $452$ $49.95$ $44.8$ $4.874$ $0$ $FGS2$ $448$ $48.74$ $44.4$ $4.722$ $0$ $FGS6$ $4444$ $47.22$ $44.8$ $4.874$ $0$ $FGS2$ $448$ $48.74$ $44.4$ $4.722$ $0$ $FGS6$ $4444$ $47.22$ $44.8$ $4.874$ $0$ $FGS12$ $448$ $48.74$ $44.4$ $4.57$ $0$ $FGS16$ $4444$ $47.22$ $44$ $4.57$ $0$ $FGS16$ $434$ $43.42$ $42.6$ $4.18$ $0$ $GS12$	47.0	5.49	0	EF314 EEQ10	470	54.9
46.8 $5.355$ 0       FS2       468 $53.55$ 46.4 $5.265$ 0       FS6       464 $52.65$ 46 $5.175$ 0       FS10       460 $51.75$ 45.6 $5.085$ 0       FS14       456 $50.85$ 45.2 $4.995$ 0       FS18 $452$ $49.95$ 44.8 $4.874$ 0       FGS2       448 $48.74$ 44.4 $4.722$ 0       FGS6       444 $47.22$ 44 $4.57$ 0       FGS10       440 $45.7$ 43.8 $4.494$ 0       FGS12 $438$ $44.94$ 43.4 $4.342$ 0       FGS12 $438$ $44.94$ 42.6 $4.18$ 0       GS4 $426$ $41.8$ 42.6 $4.18$ 0       GS12 $418$ $41.4$ 41.8 $4.14$ 0       GS12 $418$ $41.4$ 41.8 $4.14$ 0       GS16 $414$ $41.2$	41.2	5.45	U	EF310	472	54.5
40.6       3.333       0 $132$ 406 $33.33$ 46.4       5.265       0       FS6       464 $52.65$ 46       5.175       0       FS10       460 $51.75$ 45.6       5.085       0       FS14       456 $50.85$ 45.2       4.995       0       FS18 $452$ $49.95$ 44.8       4.874       0       FGS2       448 $48.74$ 44.4       4.722       0       FGS6       444 $47.22$ 44.4       4.57       0       FGS10       440 $45.7$ 43.8       4.494       0       FGS12       438 $44.94$ 43.4       4.342       0       FGS16       434 $43.42$ 42.6       4.18       0       GS4 $426$ $41.8$ 42.6       4.18       0       GS8 $422$ $41.6$ 41.8       4.14       0       GS12 $418$ $41.4$ 41.8       4.14       0       GS16 $414$ $41.2$	16.8	5 355	0	ES2	468	53 55
40.4 $0.203$ $0$ $100$ $404$ $02.03$ 46 $5.175$ $0$ FS10 $460$ $51.75$ 45.6 $5.085$ $0$ FS14 $456$ $50.85$ 45.2 $4.995$ $0$ FS14 $456$ $50.85$ 45.2 $4.995$ $0$ FS18 $452$ $49.95$ 44.8 $4.874$ $0$ FGS2 $448$ $48.74$ 44.4 $4.722$ $0$ FGS6 $444$ $47.22$ 44 $4.57$ $0$ FGS10 $440$ $45.7$ 43.8 $4.494$ $0$ FGS12 $438$ $44.94$ 43.4 $4.342$ $0$ FGS16 $434$ $43.42$ 42.6 $4.18$ $0$ GS4 $426$ $41.8$ $42.2$ $4.16$ $0$ GS12 $418$ $41.4$ $41.4$ $4.12$ $0$ GS16 $414$ $41.2$ $42.6$ $4.05$ $0$ $GS16$ $414$ $41.2$ <t< td=""><td>46.0</td><td>5.355</td><td>0</td><td>FS6</td><td>464</td><td>52.65</td></t<>	46.0	5.355	0	FS6	464	52.65
45       5.113       6       1616       466       51173         45.6       5.085       0       FS14       456       50.85         45.2       4.995       0       FS18       452       49.95         44.8       4.874       0       FGS2       448       48.74         44.4       4.722       0       FGS6       444       47.22         44       4.57       0       FGS10       440       45.7         43.8       4.494       0       FGS12       438       44.94         43.4       4.342       0       FGS16       434       43.42         42.6       4.18       0       GS4       426       41.8         42.2       4.16       0       GS12       418       41.4         41.8       4.14       0       GS12       418       41.4         41.4       4.12       0       GS16       414       41.2	46	5.205	0	FS10	460	51.75
45.0       5.005       0       FS18       452       49.95         45.2       4.995       0       FS18       452       49.95         44.8       4.874       0       FGS2       448       48.74         44.4       4.722       0       FGS6       444       47.22         44       4.57       0       FGS10       440       45.7         43.8       4.494       0       FGS12       438       44.94         43.4       4.342       0       FGS16       434       43.42         42.6       4.18       0       GS4       426       41.8         42.2       4.16       0       GS12       418       41.4         41.8       4.14       0       GS12       418       41.4         41.4       4.12       0       GS16       414       41.2	45.6	5.085	0	FS14	456	50.85
40.2       4.000       0       1010       402       4000         44.8       4.874       0       FGS2       448       48.74         44.4       4.722       0       FGS6       444       47.22         44       4.57       0       FGS10       440       45.7         43.8       4.494       0       FGS12       438       44.94         43.4       4.342       0       FGS16       434       43.42         42.6       4.18       0       GS4       426       41.8         42.6       4.18       0       GS8       422       41.6         41.8       4.14       0       GS12       418       41.4         41.4       4.12       0       GS16       414       41.2	45.0	4 995	0	FS18	450	49.95
44.8       4.874       0       FGS2       448       48.74         44.4       4.722       0       FGS6       444       47.22         44       4.57       0       FGS10       440       45.7         43.8       4.494       0       FGS12       438       44.94         43.4       4.342       0       FGS16       434       43.42         42.6       4.18       0       GS4       426       41.8         42.2       4.16       0       GS8       422       41.6         41.8       4.14       0       GS12       418       41.4         41.4       4.12       0       GS16       414       41.2	-1012	11000		1010	102	10100
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	44.8	4.874	0	FGS2	448	48.74
44       4.57       0       FGS10       440       45.7         43.8       4.494       0       FGS12       438       44.94         43.4       4.342       0       FGS16       434       43.42         42.6       4.18       0       GS4       426       41.8         42.2       4.16       0       GS8       422       41.6         41.8       4.14       0       GS12       418       41.4         41.4       4.12       0       GS16       414       41.2	44.4	4.722	0	FGS6	444	47.22
43.8       4.494       0       FGS12       438       44.94         43.4       4.342       0       FGS16       434       43.42         42.6       4.18       0       GS4       426       41.8         42.2       4.16       0       GS8       422       41.6         41.8       4.14       0       GS12       418       41.4         41.4       4.12       0       GS16       414       41.2	44	4.57	0	FGS10	440	45.7
43.4       4.342       0       FGS16       434       43.42         42.6       4.18       0       GS4       426       41.8         42.2       4.16       0       GS8       422       41.6         41.8       4.14       0       GS12       418       41.4         41.4       4.12       0       GS16       414       41.2	43.8	4.494	0	FGS12	438	44.94
42.6       4.18       0       GS4       426       41.8         42.2       4.16       0       GS8       422       41.6         41.8       4.14       0       GS12       418       41.4         41.4       4.12       0       GS16       414       41.2	43.4	4.342	0	FGS16	434	43.42
42.6       4.18       0       GS4       426       41.8         42.2       4.16       0       GS8       422       41.6         41.8       4.14       0       GS12       418       41.4         41.4       4.12       0       GS16       414       41.2			-		-	
42.2       4.16       0       GS8       422       41.6         41.8       4.14       0       GS12       418       41.4         41.4       4.12       0       GS16       414       41.2         40.8       4.05       0       GUS2       402       402	42.6	4.18	0	GS4	426	41.8
41.8         4.14         0         GS12         418         41.4           41.4         4.12         0         GS16         414         41.2	42.2	4.16	0	GS8	422	41.6
41.4 4.12 0 GS16 414 41.2	41.8	4.14	0	GS12	418	41.4
	41.4	4.12	0	GS16	414	41.2
40.0   4.00   U   GH52   408   40.5	40.8	4.05	0	GHS2	408	40.5

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
40.4	3.95	0	GHS6	404	39.5
40	3.85	0	GHS10	400	38.5
39.6	3.75	0	GHS14	396	37.5
39.2	3.65	0	GHS18	392	36.5
38.6	3.54	0	HS4	386	35.4
38.2	3.48	0	HS8	382	34.8
37.8	3.42	0	HS12	378	34.2
37.4	3.36	0	HS16	374	33.6
36.8	3.215	0	HIS2	368	32.15
36.4	3.045	0	HIS6	364	30.45
36	2.875	0	HIS10	360	28.75
35.6	2.705	0	HIS14	356	27.05
35.2	2.535	0	HIS18	352	25.35
34.6	2.43	0	IS4	346	24.3
34.2	2.41	0	IS8	342	24.1
33.8	2.39	0	IS12	338	23.9
33.4	2.37	0	IS16	334	23.7
32.8	2.315	0	IJS2	328	23.15
32.4	2.245	0	IJS6	324	22.45
32	2.175	0	IJS10	320	21.75
31.6	2.105	0	IJS14	316	21.05
31.2	2.035	0	IJS18	312	20.35
30.6	1.97	0	JS4	306	19.7
30.2	1.99	0	JS8	302	19.9
29.8	2.01	0	JS12	298	20.1
29.4	2.03	0	JS16	294	20.3
28.8	1.984	0	JKS2	288	19.84
28.4	1.852	0	JKS6	284	18.52
28	1.72	0	JKS10	280	17.2
27.6	1.588	0	JKS14	276	15.88
27.2	1.456	0	JKS18	272	14.56
26.6	1.42	0	KS4	266	14.2
26.2	1.44	0	KS8	262	14.4
25.8	1.46	0	KS12	258	14.6
25.4	1.48	0	KS16	254	14.8
24.6	1.54	0	KLS4	246	15.4
24.2	1.58	0	KLS8	242	15.8
23.8	1.62	0	KLS12	238	16.2
23.4	1.66	0	KLS16	234	16.6

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
22.8	1.74	0	LS2	228	17.4
22.4	1.82	0	LS6	224	18.2
22	1.9	0	LS10	220	19
21.6	1.98	0	LS14	216	19.8
21.2	2.06	0	LS18	212	20.6
20.6	2.1	0	LMS4	206	21
20.2	2.1	0	LMS8	202	21
19.8	2.1	0	LMS12	198	21
19.4	2.1	0	LMS16	194	21
18.8	2.196	0	MS2	188	21.96
18.4	2.388	0	MS6	184	23.88
18	2.58	0	MS10	180	25.8
17.6	2.772	0	MS14	176	27.72
17.2	2.964	0	MS18	172	29.64
16.6	3.07	0	MNS4	166	30.7
16.2	3.09	0	MNW8	162	30.9
15.8	3.11	0	MNS12	158	31.1
15.4	3.13	0	MINS16	154	31.3
44.9	2.075	•	NGO	440	22.75
14.0	3.273	0	NG2	140	32.73
14.4	3.323	0	NS0 NS10	144	33.23
14	3.775	0	NSTU NSTA	140	37.75
13.0	4.025	0	NS14 NS18	130	40.23
13.2	4.275	U	NSTO	152	42.75
12.8	4 38	0	NOS2	128	43.8
12.0	4.50	0	NOS2 NOS6	120	45.0
12	4.04	0	NOS10	124	47
11.6	4.86	0	NOS14	116	48.6
11.2	5.02	0	NOS18	112	50.2
		-			
10.9	5.17	0	OS1	109	51.7
10.7	5.31	0	OS3	107	53.1
10.4	5.5	0	OPSA1	104	55
10.2	5.6	0	OPSA3	102	56
9.9	5.73	0	OPSB1	99	57.3
9.7	5.79	0	OPSB3	97	57.9
9.3	5.93	0	OPSC2	93	59.3
9.1	6.01	0	OPSC4	91	60.1
8.9	6.09	0	OPS1	89	60.9
8.7	6.17	0	OPS3	87	61.7

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
8.4	6.28	0	OPSD1	84	62.8
8.2	6.34	0	OPSD3	82	63.4
7.8	6.44	0	OPSE2	78	64.4
7.6	6.48	0	OPSE4	76	64.8
		-			
7.3	6.5	0	OPSF2	73	65
7.1	6.5	0	OPSF4	71	65
6.9	6.51	0	PS1	69	65.1
6./	6.53	0	PS3	67	65.3
0.4	0.50		50044		05.0
6.4	6.56	0	PQSA1	64	65.6
6.2	6.58	U	PQSA3	62	65.6
<b>E</b> 0	6.60	0	DOSD1	50	66.0
<b>J.0</b>	0.02	0	PQ3D2	<u> </u>	00.2 66.4
5.0	0.04	U	FQ3D4	50	00.4
5.3	6.62	0	POSC2	52	66.3
5.3	6.61	0	POSCA	51	66 1
5.1	0.01	0	F Q 304	51	00.1
4.9	6 57	0	POS1	49	65.7
4.5	6.51	0	POS3	43	65.1
	0.01	U	1 405		00.1
4 4	64	0	PQSD1	44	64
4.2	6.3	0	PQSD3	42	63
		-			
3.8	6.1	0	PQSE2	38	61
3.6	6	0	PQSE4	36	60
3.3	5.89	0	PQSF2	33	58.9
3.1	5.83	0	PQSF4	31	58.3
2.9	5.81	0	QS1	29	58.1
2.7	5.83	0	QS3	27	58.3
2.3	5.91	0	QSA2	23	59.1
1.9	6.125	0	QSC1	19	61.25
1.66	6.6	0	QSF1	16.6	66
1.52	6.9	0	QSG2	15.2	69
1.54	7.1	0	QSH1	15.4	71
1.68	7.4	0	QSI2	16.8	74

Х	Y	Z (Velocity)	Station Name	X Plot	Y Plot
1.76	7.6	0	QTF1	17.6	76
1.7	7.77776	0	QTE12	17	77.7776
1.5	7.8148	0	QTE10	15	78.148
1.3	7.85184	0	QTE8	13	78.5184
1.1	7.88888	0	QIE6	11	78.8888
0.9	7.92592	0	QTE4	9	79.2592
0.7	7.96296	0	QTE2	1	79.6296
0.7	0.0224	0	07040	7	00.004
0.7	8.0334	0		/	80.334
0.9	0.00072	0		9	00.0072
1.1	0.10004	0		11	01.0004
1.3	0.13330	0		15	01.3330
1.5	0.10000	0	QTD2	15	01.0000
1.0	8.2	0	OTP1	10	02
1.3	0.3	0	QIDI	19	03
21	8 37	0	0744	21	83.7
2.1	8 /1	0		21	8/ 1
2.5	0.41	0	QTAZ	25	04.1
27	8 47	0	QT3	27	84 7
2.0	8 4 9	0		29	84.9
210	0110	<b>.</b>	<b>Q</b> 11	20	0110
3.1	8.52	0	PQTF4	31	85.2
3.3	8.56	0	PQTF2	33	85.6
		-			
3.6	8.61	0	PQTE4	36	86.1
3.8	8.63	0	PQTE2	38	86.3
4.2	8.79	0	PQTD3	42	87.9
4.4	8.93	0	PQTD1	44	89.3
4.7	8.94	0	PQT3	47	89.4
4.9	8.88	0	PQT1	49	88.8
5.1	8.89	0	PQTC4	51	88.9
5.3	8.97	0	PQTC2	53	89.7
5.6	9.12	0	PQTB4	56	91.2
5.8	9.26	0	PQTB2	58	92.6
6.2	9.46	0	PQTA3	62	94.6
6.4	9.52	0	PQTA1	64	95.2
6.7	9.59	0	PT3	67	95.9
6.9	9.63	0	PT1	69	96.3

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
7.1	9.66	0	OPTJ4	71	96.6
7.3	9.68	0	OPTJ2	73	96.8
7.7	9.72	0	OPTI3	77	97.2
7.9	9.74	0	OPTI1	79	97.4
8.1	9.7227	0	OPTH5	81	97.227
8.3	9.61362	0	OPTH3	83	96.1362
8.5	9.50454	0	OPTH1	85	95.0454
8.52	9.3	0	OPTG1	85.2	93
8.5	9.1	0	OPTF2	85	91
8.5	8.8	0	OPTE1	85	88
8.7	8.58	0	OPT3	87	85.8
8.9	8.56	0	OPT1	89	85.6
9.1	8.55	0	OPTC4	91	85.5
9.3	8.55	0	OPTC2	93	85.5
		-			
9.6	8.59	0	OPTB4	96	85.9
9.8	8.67	0	OPTB2	98	86.7
10.2	8.79	0	OPTA3	102	87.9
10.4	8.83	0	OPTA1	104	88.3
10.7	8.81	0	013	107	88.1
10.9	8.77	0	011	109	87.7
44.0	0.70		NOTIO	440	07.0
11.2	8.73	0	NOT18	112	87.3
11.6	8.69	0	NOT14	116	86.9
12	6.65	U	NOTIU	120	86.5
40.4	0.04	•	NOTO	404	00.4
12.4	0.01	0	NOTO NOTO	124	00.1
12.0	0.37	U	NUTZ	120	05.7
12.0	0.61	0	NT10	122	96.1
13.2	8.01	0		132	87.2
11.0	8.85	0	NT14 NT10	140	88.5
14	8 07	0	NTE	140	80.5
14.4	9.09	0	NT2	1/18	00.0
17.0	3.03		1112	170	30.3
15.2	9.175	0	MNT18	152	91 75
15.6	9.225	0	MNT14	156	92.25
16	9.275	0	MNT10	160	92.75
16.4	9.325	0	MNT6	164	93.25
L	L	-			

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
16.8	9.375	0	MNT2	168	93.75
17.2	9.3	0	MT18	172	93
17.6	9.1	0	MT14	176	91
18	8.9	0	MT10	180	89
18.4	8.7	0	MT6	184	87
18.8	8.5	0	MT2	188	85
19.4	8.4	0	LMT16	194	84
19.8	8.4	0	LMT12	198	84
20.2	8.4	0	LMT8	202	84
20.6	8.4	0	LMT4	206	84
21.4	8.4	0	LT16	214	84
21.8	8.4	0	LT12	218	84
22.2	8.4	0	LT8	222	84
22.6	8.4	0	LT4	226	84
23.4	8.4	0	KLT16	234	84
23.8	8.4	0	KLT12	238	84
24.2	8.4	0	KLT8	242	84
24.6	8.4	0	KLT4	246	84
25.4	8.4	0	KT16	254	84
25.8	8.4	0	KT12	258	84
26.2	8.4	0	KT8	262	84
26.6	8.4	0	KT4	266	84
27.4	8.43	0	JKT16	274	84.3
27.8	8.46	0	JKT12	278	84.6
28.2	8.49	0	JKT8	282	84.9
28.6	8.52	0	JKT4	286	85.2
29.4	8.55	0	JT16	294	85.5
29.8	8.55	0	JT12	298	85.5
30.2	8.55	0	JT8	302	85.5
30.6	8.55	0	JT4	306	85.5
31.2	8.59	0	IJT18	312	85.9
31.6	8.67	0	IJT14	316	86.7
32	8.75	0	IJT10	320	87.5
32.4	8.83	0	IJT6	324	88.3
32.8	8.91	0	IJT2	328	89.1
33.2	8.94	0	IT18	332	89.4
33.6	8.92	0	IT14	336	89.2
34	8.9	0	IT10	340	89
34.4	8.88	0	IT6	344	88.8

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
34.8	8.86	0	IT2	348	88.6
35	8.85	0	IT0	350	88.5
35.2	9.085	0	HIT18	352	90.85
35.6	9.155	0	HIT14	356	91.55
36	9.225	0	HIT10	360	92.25
36.4	9.295	0	HIT6	364	92.95
36.8	9.365	0	HIT2	368	93.65
37.4	9.42	0	HT16	374	94.2
37.8	9.44	0	HT12	378	94.4
38.2	9.46	0	HT8	382	94.6
38.6	9.48	0	HT4	386	94.8
39.4	9.48	0	GHT16	394	94.8
39.8	9.46	0	GHT12	398	94.6
40.2	9.44	0	GHT8	402	94.4
40.6	9.42	0	GHT4	406	94.2
41.2	9.34	0	GT18	412	93.4
41.6	9.22	0	GT14	416	92.2
42	9.1	0	GT10	420	91
42.4	8.98	0	GT6	424	89.8
42.8	8.86	0	GT2	428	88.6
43.2	8.845	0	FGT18	432	88.45
43.6	8.935	0	FGT14	436	89.35
44	9.025	0	FGT10	440	90.25
44.4	9.115	0	FGT6	444	91.15
44.8	9.205	0	FGT2	448	92.05
45.2	9.255	0	FT18	452	92.55
45.6	9.265	0	FT14	456	92.65
46	9.275	0	FT10	460	92.75
46.4	9.285	0	FT6	464	92.85
46.8	9.295	0	FT2	468	92.95
47.2	9.325	0	EFT18	472	93.25
47.6	9.375	0	EFT14	476	93.75
48	9.425	0	EFT10	480	94.25
48.4	9.475	0	EFT6	484	94.75
48.8	9.525	0	EFT2	488	95.25
49.2	9.565	0	ET18	492	95.65
49.6	9.595	0	ET14	496	95.95
50	9.625	0	ET10	500	96.25
50.4	9.655	0	ET6	504	96.55
50.8	9.685	0	ET2	508	96.85

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
51.2	9.725	0	DET18	512	97.25
51.6	9.775	0	DET14	516	97.75
52	9.825	0	DET10	520	98.25
52.4	9.875	0	DET6	524	98.75
52.8	9.925	0	DET2	528	99.25
53.2	9.975	0	DT18	532	99.75
53.6	10.025	0	DT14	536	100.25
54	10.075	0	DT10	540	100.75
54.4	10.125	0	DT6	544	101.25
54.8	10.175	0	DT2	548	101.75
55.1	10.18	0	CDTF4	551	101.8
55.3	10.14	0	CDTF2	553	101.4
55.6	10.07	0	CDTE4	556	100.7
55.8	10.01	0	CDTE2	558	100.1
56.2	9.95	0	CDTD3	562	99.5
56.4	9.95	0	CDTD1	564	99.5
56.7	9.95	0	CDT3	567	99.5
56.9	9.95	0	CDT1	569	99.5
57.1	9.96	0	CDTC4	571	99.6
57.3	9.98	0	CDTC2	573	99.8
57.6	10.01	0	CDTB4	576	100.1
57.8	10.03	0	CDTB2	578	100.3
		•		010	
58.2	10.03	0	CDTA3	582	100.3
58.4	10.00	0	CDTA1	584	100.0
00.1		<b>.</b>	<b>UD</b> I/AI	001	
58.7	9.98	0	СТЗ	587	99.8
58.9	9.96	0	CT1	589	99.6
50.5	5.50	•	011	505	55.0
50 1	9 95	0	BCTF4	501	99.5
50.3	0.05	0	BCTE2	503	00.5
59.5	9.95	0	BCTE4	595	99.5
50.8	9.92	0	BCTE2	508	99.2
53.0	3.00	0	DUTEZ	530	30.0
60.2	0 83	0	BCTD3	602	08.2
60.4	J.02	0	BCTD3	604	90.2 09.4
00.4	<b>9.04</b>	U	BUIDI	004	90.4
<u> </u>	0.05	•	DOTO	C07	00.5
00.7	9.80	U	BUIJ DOTA	007	98.5
60.9	9.85	U	BCIJ	009	98.5

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
61.1	9.9	0	BCTC4	611	99
61.3	10	0	BCTC2	613	100
61.6	10.16	0	BCTB4	616	101.6
61.8	10.28	0	BCTB2	618	102.8
62.2	10.52	0	BCTA3	622	105.2
62.4	10.64	0	BCTA1	624	106.4
62.7	10.7	0	BT3	627	107
62.9	10.7	0	BT1	629	107
63.1	10.69	0	ABTF4	631	106.9
63.3	10.67	0	ABTF2	633	106.7
63.6	10.62	0	ABTE4	636	106.2
63.8	10.53	0	ABTE2	638	105.3
64.2	10.43	0	ABTD3	642	104.3
64.4	10.41	0	ABTD1	644	104.1
64.7	10.4	0	ABT3	647	104
64.9	10.4	0	ABT1	649	104
65.1	10.42	0	ABTC4	651	104.2
65.3	10.46	0	ABTC2	653	104.6
65.6	10.49	0	ABTB4	656	104.9
65.8	10.47	0	ABTB2	658	104.7
66.2	10.35	0	ABTA3	662	103.5
66.4	10.25	0	ABTA1	664	102.5
66.7	10.12	0	AT3	667	101.2
66.9	10.04	0	AT1	669	100.4
67.1	9.98	0	AETM4	671	99.8
67.3	9.94	0	AETM2	673	99.4
67.85	9.675	0	AETK1	678.5	96.75
68.35	9.45	0	AETI1	683.5	94.5
68.7	9.38	0	AETH3	687	93.8
68.9	9.36	0	AETH1	689	93.6
69.2	9.3	0	AETG2	692	93

X	Y	Z (Velocity)	Station Name	X Plot	Y Plot
69.6	9.08888	0	AETE8	696	90.8888
69.8	9.06666	0	AETE6	698	90.6666
70	9.04444	0	AETE4	700	90.4444
70.2	9.02222	0	AETE2	702	90.2222
70.6	8.875	0	AETD2	706	88.75
70.7	8.72913	0	AETC11	707	87.2913
70.5	8.68747	0	AETC9	705	86.8747
70.3	8.64581	0	AETC7	703	86.4581
70.1	8.60415	0	AETC5	701	86.0415
69.9	8.56249	0	AETC3	699	85.6249
69.7	8.52083	0	AETC1	697	85.2083
69.63	8.4	0	AETB2	696.3	84
69.9	8.22	0	AETA1	699	82.2
70.05	8.1	0	AET1	700.5	81

CALIE	BRATION CERTIFIC	CATE												
Model: 2000	Serial Number: 200 2679													
		stant												
	Type of Reading													
Velocity:	Level:													
СМЗ	-													
U		Le N/A												
Static Veloc	ity Dynamic Velocity	Level												
Standard: Zero	2.00	NA												
Measured: 0,00	2.00	NA												
X Factory Calibration														
Field Profile Calibration	n;													
Site Coefficient or Velo	city Multiplier:													
Calibration Technician:	h	Date: <u>4-20-07</u>												
QA Technician:	A.	Date: 2014												
This document certifies that Verification is indicated by is traceable to the National Gaithersburg, MD. For proo	t the described instrument in the measured results show a Institute of Standards and T duct information, service, or artment	as been calibrated. above. Velocity calibration Fechnology (NIST), calibration, please contact												
the Customer Service Depa														
	MARSH MCBIRNEY A Higher Level of Flow Measurement													
4539 Metro (301) 874-5599	politan Ct., Frederick, MD 2 9 • (800)-368-2723 • FAX ( www.marsh-mcbirney.com	21704-9452 301) 874-2172												
SUMMARY OF DISCHARGE MEASUREMENT ACTIVITIES														
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MAMMOTH	Ма	Marion County, Florida												
Performed by Karst Environmental Services, Inc., High Springs, Florida														
DATE	DISCHARGE	INSTR.	CALC.	NUMBER	X-SECTION	Avg. Station	High	Low	TIME	TIME	Depth	Neg.	Blanking	NOTES:
	(CFS)	USED	METHOD	STATIONS	AREA	Point Velocity	Msmt.	Msmt.	START:	FINISH:		PV's	Used?	
					(sq.feet)	(fps)	(fps)	(fps)			(feet)			
3/24/2005	300.29	MMB 201	Grid Count	115	323.06	0.96	1.33	-0.14	14:00	17:50	25-34	3	yes	
9/19/2006	240.07	MMB 201	Grid Count	138	308.16	0.71	1.16	-0.39	13:40	17:50	26-32	8	yes	
9/10/2007	207.78	MMB 201	Grid Count	132	321.36	0.61	0.96	-0.06	12:50	16:42	26-34	2	yes	